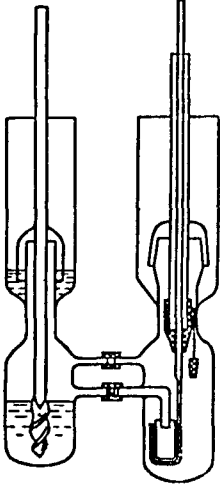


|  |        |                     |  |                               |                 |
|--|--------|---------------------|--|-------------------------------|-----------------|
| <b>COMPONENTS:</b><br>(1) Potassium bromate; $\text{KBrO}_3$ ; [7758-01-2]<br>(2) Water; $\text{H}_2\text{O}$ ; [7732-18-5]  |        |                     | <b>ORIGINAL MEASUREMENTS:</b><br>Ricci, J.E.<br><i>J. Am. Chem. Soc.</i> <u>1934</u> , 56, 299-303.  |                               |                 |
| <b>VARIABLES:</b><br>T/K = 278 - 323   |        |                     | <b>PREPARED BY:</b><br>Hiroshi Miyamoto  |                               |                 |
| <b>EXPERIMENTAL VALUES:</b> Solubility of $\text{KBrO}_3$  |        |                     |  |                               |                 |
| $t/^\circ\text{C}$   | mass % | mol %<br>(compiler) | mol $\text{kg}^{-1}$<br>(compiler)   | Density<br>$\text{g cm}^{-3}$ | Solid phase     |
| 5  | 3.642  | 0.4061              | 0.2263   | 1.024                         | $\text{KBrO}_3$ |
| 10   | 4.510  | 0.5069              | 0.2828   | 1.035                         | "               |
| 15   | 5.397  | 0.6117              | 0.3416   | 1.042                         | "               |
| 20   | 6.460  | 0.7395              | 0.4135   | 1.048                         | "               |
| 25   | 7.533  | 0.8712              | 0.4878   | 1.054                         | "               |
| 30   | 8.785  | 1.028               | 0.5767   | 1.062                         | "               |
| 35   | 10.13  | 1.201               | 0.6750   | 1.074                         | "               |
| 40   | 11.58  | 1.393               | 0.7842   | 1.083                         | "               |
| 45   | 13.08  | 1.597               | 0.9011   | -                             | "               |
| 50   | 14.69  | 1.824               | 1.031  | -                             | "               |
| <b>AUXILIARY INFORMATION</b>   |        |                     |  |                               |                 |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Mixtures of $\text{KBrO}_3$ and water were placed in bottles and rotated in a large water thermostat for two days, a time found to be sufficient for attaining equilibrium. Samples of the saturated solution were withdrawn by means of a calibrated pipet provided with a folded filter paper at the tip. The bromate was determined by titration with standard sodium thiosulfate solution. |        |                     | <b>SOURCE AND PURITY OF MATERIALS:</b><br>C.p. grade $\text{KBrO}_3$ was recrystallized, dried to the anhydrous state, and stored in a $100^\circ\text{C}$ oven. |                               |                 |
|  |        |                     | <b>ESTIMATED ERROR:</b><br>Soly: accuracy within 0.2 %.<br>Temp: precision $\pm 0.01$ K.<br>Densities: precision about 0.1 %.                                    |                               |                 |
|  |        |                     | <b>REFERENCES:</b>   |                               |                 |

| <b>COMPONENTS:</b><br>(1) Potassium bromate; $\text{KBrO}_3$ ; [7758-01-2]<br>(2) Water; $\text{H}_2\text{O}$ ; [7732-18-5]  | <b>ORIGINAL MEASUREMENTS:</b><br>Benrath, A.; Gjedebo, F.; Schiffers, B.; Wunderlich, H.<br><i>Z. Anorg. Allg. Chem.</i> <u>1937</u> , 231, 285-97.  |  |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
|--|--|--|--------|--|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|-----|------|------|
| <b>VARIABLES:</b><br>T/K = 407 to 585  | <b>PREPARED BY:</b><br>Hiroshi Miyamoto  |  |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| <b>EXPERIMENTAL VALUES:</b> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;"><math>t/^\circ\text{C}</math></th> <th style="text-align: center;">mass %</th> <th style="text-align: center;">Solubility<br/>mol <math>\text{kg}^{-1}</math><br/>(compiler)</th> </tr> </thead> <tbody> <tr><td style="text-align: center;">134</td><td style="text-align: center;">43.6</td><td style="text-align: center;">4.63</td></tr> <tr><td style="text-align: center;">149</td><td style="text-align: center;">48.4</td><td style="text-align: center;">5.62</td></tr> <tr><td style="text-align: center;">160</td><td style="text-align: center;">51.1</td><td style="text-align: center;">6.26</td></tr> <tr><td style="text-align: center;">167</td><td style="text-align: center;">53.5</td><td style="text-align: center;">6.89</td></tr> <tr><td style="text-align: center;">170</td><td style="text-align: center;">54.1</td><td style="text-align: center;">7.06</td></tr> <tr><td style="text-align: center;">172</td><td style="text-align: center;">57.3</td><td style="text-align: center;">8.04</td></tr> <tr><td style="text-align: center;">186</td><td style="text-align: center;">59.9</td><td style="text-align: center;">8.94</td></tr> <tr><td style="text-align: center;">193</td><td style="text-align: center;">63.2</td><td style="text-align: center;">10.3</td></tr> <tr><td style="text-align: center;">204</td><td style="text-align: center;">64.2</td><td style="text-align: center;">10.7</td></tr> <tr><td style="text-align: center;">211</td><td style="text-align: center;">67.4</td><td style="text-align: center;">12.4</td></tr> <tr><td style="text-align: center;">226</td><td style="text-align: center;">70.6</td><td style="text-align: center;">14.4</td></tr> <tr><td style="text-align: center;">230</td><td style="text-align: center;">72.6</td><td style="text-align: center;">15.9</td></tr> <tr><td style="text-align: center;">249</td><td style="text-align: center;">72.6</td><td style="text-align: center;">15.9</td></tr> <tr><td style="text-align: center;">254</td><td style="text-align: center;">74.4</td><td style="text-align: center;">17.4</td></tr> <tr><td style="text-align: center;">265</td><td style="text-align: center;">77.2</td><td style="text-align: center;">20.3</td></tr> <tr><td style="text-align: center;">274</td><td style="text-align: center;">79.1</td><td style="text-align: center;">22.7</td></tr> <tr><td style="text-align: center;">279</td><td style="text-align: center;">81.1</td><td style="text-align: center;">25.7</td></tr> <tr><td style="text-align: center;">286</td><td style="text-align: center;">81.4</td><td style="text-align: center;">26.2</td></tr> <tr><td style="text-align: center;">297</td><td style="text-align: center;">83.1</td><td style="text-align: center;">29.4</td></tr> <tr><td style="text-align: center;">312</td><td style="text-align: center;">86.4</td><td style="text-align: center;">38.0</td></tr> </tbody> </table> |  | $t/^\circ\text{C}$                               | mass % | Solubility<br>mol $\text{kg}^{-1}$<br>(compiler) | 134 | 43.6 | 4.63 | 149 | 48.4 | 5.62 | 160 | 51.1 | 6.26 | 167 | 53.5 | 6.89 | 170 | 54.1 | 7.06 | 172 | 57.3 | 8.04 | 186 | 59.9 | 8.94 | 193 | 63.2 | 10.3 | 204 | 64.2 | 10.7 | 211 | 67.4 | 12.4 | 226 | 70.6 | 14.4 | 230 | 72.6 | 15.9 | 249 | 72.6 | 15.9 | 254 | 74.4 | 17.4 | 265 | 77.2 | 20.3 | 274 | 79.1 | 22.7 | 279 | 81.1 | 25.7 | 286 | 81.4 | 26.2 | 297 | 83.1 | 29.4 | 312 | 86.4 | 38.0 |
| $t/^\circ\text{C}$   | mass %   | Solubility<br>mol $\text{kg}^{-1}$<br>(compiler) |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 134  | 43.6   | 4.63   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 149  | 48.4   | 5.62   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 160  | 51.1   | 6.26   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 167  | 53.5   | 6.89   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 170  | 54.1   | 7.06   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 172  | 57.3   | 8.04   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 186  | 59.9   | 8.94   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 193  | 63.2   | 10.3   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 204  | 64.2   | 10.7   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 211  | 67.4   | 12.4   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 226  | 70.6   | 14.4   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 230  | 72.6   | 15.9   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 249  | 72.6   | 15.9   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 254  | 74.4   | 17.4   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 265  | 77.2   | 20.3   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 274  | 79.1   | 22.7   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 279  | 81.1   | 25.7   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 286  | 81.4   | 26.2   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 297  | 83.1   | 29.4   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| 312  | 86.4   | 38.0   |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| <b>AUXILIARY INFORMATION</b>   |  |  |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Synthetic method used with visual observation of temperature of crystallization and solubilization (ref 1). The weighed salt and water were placed in a small tube. The tubes were set in an oven equipped with a mica window. A thermometer was immersed in the oven.   | <b>SOURCE AND PURITY OF MATERIALS:</b><br>No information was given.<br><br><b>ESTIMATED ERROR:</b><br>Nothing specified.<br><br><b>REFERENCES:</b><br>1. Jaenecke, E. <i>Z. Physik. Chem.</i> <u>1936</u> , A177, 7. |  |        |  |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |     |      |      |

| <b>COMPONENTS:</b><br>(1) Potassium bromate; $\text{KBrO}_3$ ; [7758-01-2]<br>(2) Water; $\text{H}_2\text{O}$ ; [7732-18-5]  | <b>ORIGINAL MEASUREMENTS:</b><br>Breusov, O. N.; Kashina, N. I.; Revzina, T. V.; Sobolevskaya, N. G.<br><br><i>Zh. Neorg. Khim.</i> 1967, 12, 2240-3;<br><i>Russ. J. Inorg. Chem. (Engl. Transl.)</i> 1967, 12, 1179-81.   |        |                                 |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
|--|--|--------|---------------------------------|--|--|--------|-------|----------------------|---|------|--------|--------|----|------|--------|--------|----|------|--------|--------|----|------|--------|--------|----|------|-------|--------|----|-------|-------|--------|----|-------|-------|-------|----|-------|-------|-------|----|-------|-------|-------|----|-------|-------|-------|----|-------|-------|-------|-----|-------|-------|-------|
| <b>VARIABLES:</b><br>T/K = 273 to 373  | <b>PREPARED BY:</b><br>M. Salomon and H. Miyamoto  |        |                                 |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| <b>EXPERIMENTAL VALUES:</b><br><table style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th rowspan="2">t/°C</th> <th colspan="3">Solubility of <math>\text{KBrO}_3^a</math></th> </tr> <tr> <th>mass %</th> <th>mol %</th> <th>mol <math>\text{kg}^{-1}</math></th> </tr> </thead> <tbody> <tr><td>0</td><td>2.98</td><td>0.3303</td><td>0.1839</td></tr> <tr><td>10</td><td>4.54</td><td>0.5104</td><td>0.2848</td></tr> <tr><td>20</td><td>6.42</td><td>0.7346</td><td>0.4108</td></tr> <tr><td>25</td><td>7.55</td><td>0.8733</td><td>0.4890</td></tr> <tr><td>30</td><td>8.84</td><td>1.035</td><td>0.5806</td></tr> <tr><td>40</td><td>11.67</td><td>1.405</td><td>0.7911</td></tr> <tr><td>50</td><td>14.82</td><td>1.842</td><td>1.042</td></tr> <tr><td>60</td><td>18.08</td><td>2.325</td><td>1.322</td></tr> <tr><td>70</td><td>21.76</td><td>2.913</td><td>1.665</td></tr> <tr><td>80</td><td>25.35</td><td>3.534</td><td>2.033</td></tr> <tr><td>90</td><td>29.40</td><td>4.299</td><td>2.494</td></tr> <tr><td>100</td><td>33.31</td><td>5.113</td><td>2.991</td></tr> </tbody> </table> <p><sup>a</sup>Mol % and mol <math>\text{kg}^{-1}</math> solubilities calcd by compilers.</p> <div style="text-align: right; margin-top: 20px;">  </div> |  | t/°C   | Solubility of $\text{KBrO}_3^a$ |  |  | mass % | mol % | mol $\text{kg}^{-1}$ | 0 | 2.98 | 0.3303 | 0.1839 | 10 | 4.54 | 0.5104 | 0.2848 | 20 | 6.42 | 0.7346 | 0.4108 | 25 | 7.55 | 0.8733 | 0.4890 | 30 | 8.84 | 1.035 | 0.5806 | 40 | 11.67 | 1.405 | 0.7911 | 50 | 14.82 | 1.842 | 1.042 | 60 | 18.08 | 2.325 | 1.322 | 70 | 21.76 | 2.913 | 1.665 | 80 | 25.35 | 3.534 | 2.033 | 90 | 29.40 | 4.299 | 2.494 | 100 | 33.31 | 5.113 | 2.991 |
| t/°C   | Solubility of $\text{KBrO}_3^a$  |        |                                 |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
|  | mass %   | mol %  | mol $\text{kg}^{-1}$            |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 0  | 2.98   | 0.3303 | 0.1839                          |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 10   | 4.54   | 0.5104 | 0.2848                          |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 20   | 6.42   | 0.7346 | 0.4108                          |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 25   | 7.55   | 0.8733 | 0.4890                          |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 30   | 8.84   | 1.035  | 0.5806                          |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 40   | 11.67  | 1.405  | 0.7911                          |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 50   | 14.82  | 1.842  | 1.042                           |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 60   | 18.08  | 2.325  | 1.322                           |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 70   | 21.76  | 2.913  | 1.665                           |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 80   | 25.35  | 3.534  | 2.033                           |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 90   | 29.40  | 4.299  | 2.494                           |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| 100  | 33.31  | 5.113  | 2.991                           |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| <b>AUXILIARY INFORMATION</b>   |  |        |                                 |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Isothermal method. Equilibrium reached in 4-5 h. From 90-100°C, the solubility was determined in the apparatus shown in the figure. At equilibrium the apparatus was tilted to allow saturated solution to filter through connecting tube into weighed test tubes. The test tubes were closed with a stopper, withdrawn and weighed. Condensation on the walls of the apparatus and loss of water by evaporation was thus prevented. At the lower temperatures, ordinary solubility vessels were used, and pipets with glass filters were used for sampling (no other details given). Above 50°C, the pipets were preheated in the thermostat.<br><br>Bromate was determined iodometrically.   | <b>SOURCE AND PURITY OF MATERIALS:</b><br>Results of analysis of $\text{KBrO}_3$ :<br>content of $\text{KBrO}_3$ = 99.3 %, and impurities are Rb (0.1 %), Cs (0.01 %), Na (0.016 %), $\text{SO}_4$ (0.005 %), and Fe (0.0001 %).<br><br>The alkali metal impurities were dtd by flame photometry, the iron colorimetrically, and sulfate nephelometrically.<br><br><b>ESTIMATED ERROR:</b><br>Soly: nothing specified.<br><br>Temp: precision $\pm 0.1$ K.<br><br><b>REFERENCES:</b> |        |                                 |  |  |        |       |                      |   |      |        |        |    |      |        |        |    |      |        |        |    |      |        |        |    |      |       |        |    |       |       |        |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |    |       |       |       |     |       |       |       |

| <b>COMPONENTS:</b><br>(1) Potassium bromate; $\text{KBrO}_3$ ; [7758-01-2]<br>(2) Water- $\text{d}_2$ ; $\text{D}_2\text{O}$ ; [7789-20-0]<br>(3) Water; $\text{H}_2\text{O}$ ; [7732-18-5]   | <b>ORIGINAL MEASUREMENTS:</b><br>Chang, T.L.; Hsieh, Y.Y.<br><i>Sci. Repts. Natl. Tsing Hua Univ.</i><br><u>1948</u> , A5, 252-9.  |  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
|---|--|--|------------------------------|--|----|---|-------|-------|------------------------|------|------|-------|-------|-----------|------|------|-------|-------|-----------|-----|-----|--------------------|
| <b>VARIABLES:</b><br>T/K = 298.15   | <b>PREPARED BY:</b><br>G. Jansco and H. Miyamoto   |  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
| <b>EXPERIMENTAL VALUES:</b> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;"><math>t/^\circ\text{C}</math></th> <th style="text-align: center;">Water-<math>\text{d}_2</math><br/>mol %</th> <th style="text-align: center;">Potassium Bromate<br/>mole/55.51 moles of <math>\text{H}_2\text{O}-\text{D}_2\text{O}</math> mixture</th> </tr> </thead> <tbody> <tr> <td rowspan="3" style="text-align: center; vertical-align: middle;">25</td> <td rowspan="3" style="text-align: center; vertical-align: middle;">0</td> <td style="text-align: center;">0.494</td> </tr> <tr> <td style="text-align: center;">0.495</td> </tr> <tr> <td style="text-align: center;">(Av)0.495<sup>a</sup></td> </tr> <tr> <td rowspan="3" style="text-align: center; vertical-align: middle;">32.5</td> <td rowspan="3" style="text-align: center; vertical-align: middle;">32.5</td> <td style="text-align: center;">0.479</td> </tr> <tr> <td style="text-align: center;">0.479</td> </tr> <tr> <td style="text-align: center;">(Av)0.479</td> </tr> <tr> <td rowspan="3" style="text-align: center; vertical-align: middle;">66.2</td> <td rowspan="3" style="text-align: center; vertical-align: middle;">66.2</td> <td style="text-align: center;">0.460</td> </tr> <tr> <td style="text-align: center;">0.458</td> </tr> <tr> <td style="text-align: center;">(Av)0.459</td> </tr> <tr> <td rowspan="2" style="text-align: center; vertical-align: middle;">100</td> <td rowspan="2" style="text-align: center; vertical-align: middle;">100</td> <td style="text-align: center;">0.443<sup>b</sup></td> </tr> </tbody> </table> <p><sup>a</sup> Average values calculated by compiler.</p> <p><sup>b</sup> The solubility in 100 % <math>\text{D}_2\text{O}</math> was obtained from the solubilities in the <math>\text{H}_2\text{O}-\text{D}_2\text{O}</math> mixtures by linear extrapolation.</p> |  | $t/^\circ\text{C}$   | Water- $\text{d}_2$<br>mol % | Potassium Bromate<br>mole/55.51 moles of $\text{H}_2\text{O}-\text{D}_2\text{O}$ mixture | 25 | 0 | 0.494 | 0.495 | (Av)0.495 <sup>a</sup> | 32.5 | 32.5 | 0.479 | 0.479 | (Av)0.479 | 66.2 | 66.2 | 0.460 | 0.458 | (Av)0.459 | 100 | 100 | 0.443 <sup>b</sup> |
| $t/^\circ\text{C}$  | Water- $\text{d}_2$<br>mol %   | Potassium Bromate<br>mole/55.51 moles of $\text{H}_2\text{O}-\text{D}_2\text{O}$ mixture |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
| 25  | 0  | 0.494  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
|   |  | 0.495  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
|   |  | (Av)0.495 <sup>a</sup>   |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
| 32.5  | 32.5   | 0.479  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
|   |  | 0.479  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
|   |  | (Av)0.479  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
| 66.2  | 66.2   | 0.460  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
|   |  | 0.458  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
|   |  | (Av)0.459  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
| 100   | 100  | 0.443 <sup>b</sup>   |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
|   |  | <b>AUXILIARY INFORMATION</b>   |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Saturated solutions of $\text{KBrO}_3$ in the $\text{H}_2\text{O}-\text{D}_2\text{O}$ mixtures were prepared by the method of supersaturation. The supersaturated solutions were prepared by agitating excess salt with the water mixture for one hour at $60^\circ\text{C}$ ; the time of agitation in the $25^\circ\text{C}$ bath was 3 hours. A sample of the clear solution was delivered into a weighing bottle, the solvent evaporated and the residual pure salt was dried in vacuum at $100^\circ\text{C}$ and weighed.   | <b>SOURCE AND PURITY OF MATERIALS:</b><br>Potassium bromate was purified by recrystallization from conductivity water and found to be free from bromide. The salt was dried over calcium chloride in a desiccator for several days before use. $\text{D}_2\text{O}$ content of the water mixture was determined by pycnometer both before and after each measurement. The mole percentage was calculated from the specific gravity at $25^\circ\text{C}$ (ref 1).<br><br><b>ESTIMATED ERROR:</b><br>Soly: accuracy about 1 % (authors).<br>Temp: precision $\pm 0.03$ K.<br><br><b>REFERENCES:</b><br>1. Swift, E. Jr. <i>J. Am. Chem. Soc.</i> <u>1939</u> , 61, 198. |  |                              |  |    |   |       |       |                        |      |      |       |       |           |      |      |       |       |           |     |     |                    |