

| <b>COMPONENTS:</b><br>(1) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]<br>(2) Di sodium (I-4)-tetraoxomolybdate (2-) (disodium molybdate); Na <sub>2</sub> MoO <sub>4</sub> ; [7631-95-0]<br>(3) Water; H <sub>2</sub> O; [7732-18-5]  | <b>ORIGINAL MEASUREMENTS:</b><br>Ricci, J.E.; Linke, W.F.<br><br><i>J. Am. Chem. Soc.</i> <u>1947</u> , 69, 1080-3.  |                                    |                     |                               |  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
|--|--|------------------------------------|---------------------|-------------------------------|--|--|--|----------------------------------|--|-------------------|--|-------------------------------|--|--------|---------------------|--------|---------------------|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|-----|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|------|-------|------|-------|-------|---|------|-------|-------------------|-------|-------|---|
| <b>VARIABLES:</b><br>Composition at 298.2 K  | <b>PREPARED BY:</b><br>Hiroshi Miyamoto  |                                    |                     |                               |  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| <b>EXPERIMENTAL VALUES:</b> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="6" style="text-align: center;">Composition of saturated solutions</th> </tr> <tr> <th colspan="2" style="text-align: center;">Na<sub>2</sub>MoO<sub>4</sub></th> <th colspan="2" style="text-align: center;">NaIO<sub>3</sub></th> <th rowspan="2" style="text-align: center;">Density<br/>g cm<sup>-3</sup></th> <th rowspan="2" style="text-align: center;">Nature of<br/>the solid<br/>phase<sup>a</sup></th> </tr> <tr> <th style="text-align: center;">mass %</th> <th style="text-align: center;">mol %<br/>(compiler)</th> <th style="text-align: center;">mass %</th> <th style="text-align: center;">mol %<br/>(compiler)</th> </tr> </thead> <tbody> <tr><td>39.38</td><td>5.378</td><td>0.00</td><td>0.000</td><td>1.432</td><td>A</td></tr> <tr><td>39.16</td><td>5.375</td><td>0.58</td><td>0.083</td><td>1.437</td><td>"</td></tr> <tr><td>38.63</td><td>5.354</td><td>1.79</td><td>0.258</td><td>1.450</td><td>"</td></tr> <tr><td>38.46</td><td>5.349</td><td>2.20</td><td>0.318</td><td>1.453</td><td>A+B</td></tr> <tr><td>38.51</td><td>5.358</td><td>2.18</td><td>0.316</td><td>1.452</td><td>"</td></tr> <tr><td>38.43</td><td>5.343</td><td>2.21</td><td>0.320</td><td>1.451</td><td>"</td></tr> <tr><td>38.43</td><td>5.343</td><td>2.21</td><td>0.320</td><td>1.454</td><td>"</td></tr> <tr><td>38.47</td><td>5.350</td><td>2.18</td><td>0.315</td><td>1.455</td><td>"</td></tr> <tr><td>38.46</td><td>5.349</td><td>2.20</td><td>0.318</td><td>1.453</td><td>"</td></tr> <tr><td>37.23</td><td>5.090</td><td>2.24</td><td>0.319</td><td>1.436</td><td>B</td></tr> <tr><td>31.49</td><td>3.995</td><td>2.54</td><td>0.335</td><td>1.368</td><td>"</td></tr> <tr><td>24.24</td><td>2.825</td><td>3.08</td><td>0.373</td><td>1.277</td><td>"</td></tr> <tr><td>17.89</td><td>1.943</td><td>3.42</td><td>0.386</td><td>1.204</td><td>"</td></tr> <tr><td>11.41</td><td>1.163</td><td>4.16</td><td>0.441</td><td>1.143</td><td>"</td></tr> <tr><td>5.57</td><td>0.543</td><td>5.67</td><td>0.575</td><td>1.099</td><td>"</td></tr> <tr><td>0.00</td><td>0.000</td><td>8.49<sup>b</sup></td><td>0.838</td><td>1.074</td><td>"</td></tr> </tbody> </table> <p><sup>a</sup> A = Na<sub>2</sub>MoO<sub>4</sub>·2H<sub>2</sub>O;    B = NaIO<sub>3</sub>·H<sub>2</sub>O</p> <p><sup>b</sup> For the binary system the compiler computes the following:<br/>           soly of NaIO<sub>3</sub> = 0.469 mol kg<sup>-1</sup></p> |  | Composition of saturated solutions |                     |                               |  |  |  | Na <sub>2</sub> MoO <sub>4</sub> |  | NaIO <sub>3</sub> |  | Density<br>g cm <sup>-3</sup> | Nature of<br>the solid<br>phase <sup>a</sup> | mass % | mol %<br>(compiler) | mass % | mol %<br>(compiler) | 39.38 | 5.378 | 0.00 | 0.000 | 1.432 | A | 39.16 | 5.375 | 0.58 | 0.083 | 1.437 | " | 38.63 | 5.354 | 1.79 | 0.258 | 1.450 | " | 38.46 | 5.349 | 2.20 | 0.318 | 1.453 | A+B | 38.51 | 5.358 | 2.18 | 0.316 | 1.452 | " | 38.43 | 5.343 | 2.21 | 0.320 | 1.451 | " | 38.43 | 5.343 | 2.21 | 0.320 | 1.454 | " | 38.47 | 5.350 | 2.18 | 0.315 | 1.455 | " | 38.46 | 5.349 | 2.20 | 0.318 | 1.453 | " | 37.23 | 5.090 | 2.24 | 0.319 | 1.436 | B | 31.49 | 3.995 | 2.54 | 0.335 | 1.368 | " | 24.24 | 2.825 | 3.08 | 0.373 | 1.277 | " | 17.89 | 1.943 | 3.42 | 0.386 | 1.204 | " | 11.41 | 1.163 | 4.16 | 0.441 | 1.143 | " | 5.57 | 0.543 | 5.67 | 0.575 | 1.099 | " | 0.00 | 0.000 | 8.49 <sup>b</sup> | 0.838 | 1.074 | " |
| Composition of saturated solutions   |  |                                    |                     |                               |  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| Na <sub>2</sub> MoO <sub>4</sub>   |  | NaIO <sub>3</sub>                  |                     | Density<br>g cm <sup>-3</sup> | Nature of<br>the solid<br>phase <sup>a</sup> |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| mass %   | mol %<br>(compiler)  | mass %                             | mol %<br>(compiler) |                               |  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 39.38  | 5.378  | 0.00                               | 0.000               | 1.432                         | A  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 39.16  | 5.375  | 0.58                               | 0.083               | 1.437                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 38.63  | 5.354  | 1.79                               | 0.258               | 1.450                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 38.46  | 5.349  | 2.20                               | 0.318               | 1.453                         | A+B  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 38.51  | 5.358  | 2.18                               | 0.316               | 1.452                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 38.43  | 5.343  | 2.21                               | 0.320               | 1.451                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 38.43  | 5.343  | 2.21                               | 0.320               | 1.454                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 38.47  | 5.350  | 2.18                               | 0.315               | 1.455                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 38.46  | 5.349  | 2.20                               | 0.318               | 1.453                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 37.23  | 5.090  | 2.24                               | 0.319               | 1.436                         | B  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 31.49  | 3.995  | 2.54                               | 0.335               | 1.368                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 24.24  | 2.825  | 3.08                               | 0.373               | 1.277                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 17.89  | 1.943  | 3.42                               | 0.386               | 1.204                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 11.41  | 1.163  | 4.16                               | 0.441               | 1.143                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 5.57   | 0.543  | 5.67                               | 0.575               | 1.099                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| 0.00   | 0.000  | 8.49 <sup>b</sup>                  | 0.838               | 1.074                         | "  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| <b>AUXILIARY INFORMATION</b>   |  |                                    |                     |                               |  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Solubilities determined isothermally by stirring complexes of known compositions in Pyrex tubes, and sampling the equilibrated solutions by means of calibrated pipets fitted with filtering tips. Total solids were determined by evaporation of an aliquot of saturated solution and drying to constant weight at 125°C.<br><br>The iodate content in the saturated solution was determined iodometrically. A large excess of acid (HCl) was necessary to obtain the correct end-point within the short titration time in the presence of the molybdate.   | <b>SOURCE AND PURITY OF MATERIALS:</b><br>C.p. grade sodium molybdate dihydrate completely dehydrated by heating to 180°C, and stored at 150°C. The purity of this anhydrous salt was found to be 100.0%. C.p. grade sodium iodate was found to be pure within 1/1000. |                                    |                     |                               |  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |
| <b>ESTIMATED ERROR:</b><br>Soly: the accuracy of titrations was within 0.1%.<br>Temp: precision ± 0.04 K.  | <b>COMMENTS AND/OR ADDITIONAL DATA:</b><br>  |                                    |                     |                               |  |  |  |                                  |  |                   |  |                               |  |        |                     |        |                     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |      |       |      |       |       |   |      |       |                   |       |       |   |

|  |                    |                     |   |                     |  |
|--|--------------------|---------------------|---|---------------------|--|
| <b>COMPONENTS:</b><br>(1) Sodium carbonate; $\text{Na}_2\text{CO}_3$ ; [4917-19-8]<br>(2) Sodium iodate; $\text{NaIO}_3$ ; [7681-55-2]<br>(3) Water; $\text{H}_2\text{O}$ ; [7732-18-5]  |                    |                     | <b>ORIGINAL MEASUREMENTS:</b><br>Foote, H.W.; Vance, J.E.<br><i>Am. J. Sci.</i> <u>1933</u> , 25, 499-502.                            |                     |  |
| <b>VARIABLES:</b><br>Composition<br>T/K = 273 - 323  |                    |                     | <b>PREPARED BY:</b><br>Hiroshi Miyamoto   |                     |  |
| <b>EXPERIMENTAL VALUES:</b>  |                    |                     |   |                     |  |
| Composition of saturated solutions   |                    |                     |   |                     |  |
| $t/^\circ\text{C}$   | $\text{NaIO}_3$    |                     | $\text{Na}_2\text{CO}_3$  |                     | Nature of the solid phase <sup>a</sup> |
|  | mass %             | mol %<br>(compiler) | mass %  | mol %<br>(compiler) |  |
| 0  | -                  | -                   | 6.42  | 1.15                | A                                      |
|  | 0.81               | 0.078               | 6.30  | 1.14                | A+C                                    |
|  | 0.83               | 0.080               | 6.27  | 1.13                | "                                      |
|  | 2.42 <sup>b</sup>  | 0.225               | -   | -                   | C                                      |
| 25   | -                  | -                   | 22.60   | 4.728               | A                                      |
|  | 0.52               | 0.059               | 22.44   | 4.715               | "                                      |
|  | 2.16               | 0.247               | 22.22   | 4.745               | A+D                                    |
|  | 2.17               | 0.248               | 22.22   | 4.746               | "                                      |
|  | 2.54               | 0.282               | 18.82   | 3.898               | D                                      |
|  | 8.66 <sup>b</sup>  | 0.856               | -   | -                   | "                                      |
| 40   | -                  | -                   | 32.83   | 7.670               | B                                      |
|  | 0.50               | 0.063               | 32.67   | 7.667               | "                                      |
|  | 1.79               | 0.227               | 32.09   | 7.603               | B+D                                    |
|  | 1.75               | 0.222               | 32.00   | 7.570               | "                                      |
|  | 2.00               | 0.248               | 29.87   | 6.918               | D                                      |
|  | 11.71 <sup>b</sup> | 1.193               | -   | -                   | "                                      |
| continued.....   |                    |                     |   |                     |  |
| <b>AUXILIARY INFORMATION</b>   |                    |                     |   |                     |  |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Sodium iodate, sodium carbonate and water were placed in glass stoppered bottles and rotated in a thermostat. Twenty-four hours were allowed for the attainment of equilibrium at which time samples of the solution were drawn off through glass wool filters for analysis.<br>Sodium iodate content was determined by adding excess KI, acidifying with sulfuric acid, and titrating the liberated iodine with thio-sulfate solution. Sodium carbonate was detd in a second sample by titration with HCl using methyl orange indicator. In these carbonate titrations, a constant light source was used and the end point was compared with a standard made by saturating water containing a few drops of methyl orange with carbon dioxide.<br>The composition of the dry solid phase was determined by the method of Schreinemakers. |                    |                     | <b>SOURCE AND PURITY OF MATERIALS:</b><br>The authors only state that sodium iodate and carbonate were purified by customary methods. |                     |  |
|  |                    |                     | <b>ESTIMATED ERROR:</b><br>Nothing specified.   |                     |  |
|  |                    |                     | <b>REFERENCES:</b>  |                     |  |

## COMPONENTS:

- (1) Sodium carbonate;  $\text{Na}_2\text{CO}_3$ ; [4917-19-8]  
 (2) Sodium iodate;  $\text{NaIO}_3$ ; [7681-55-2]  
 (3) Water;  $\text{H}_2\text{O}$ ; [7732-18-5]

## ORIGINAL MEASUREMENTS:

Foote, H.W.; Vance, J.E.  
*Am. J. Sci.* 1933, 25, 499-502.

## EXPERIMENTAL VALUES: (Continued)

| t/°C | Composition of saturated solutions |                     |                                 |                     | Nature of the solid phase <sup>a</sup> |
|------|------------------------------------|---------------------|---------------------------------|---------------------|--|
|      | mass % $\text{NaIO}_3$             | mol %<br>(compiler) | mass % $\text{Na}_2\text{CO}_3$ | mol %<br>(compiler) |  |
| 50   | -                                  | -                   | 32.16                           | 7.457               | B                                      |
|      | 1.30                               | 0.163               | 31.52                           | 7.374               | "                                      |
|      | 2.42                               | 0.307               | 31.31                           | 7.411               | B+D                                    |
|      | 2.54                               | 0.322               | 31.23                           | 7.396               | "                                      |
|      | 3.34                               | 0.401               | 25.44                           | 5.701               | D                                      |
|      | 14.06                              | 1.468               | -                               | -                   | "                                      |

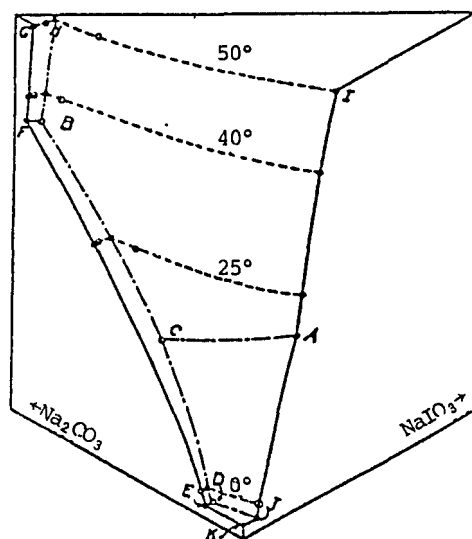
<sup>a</sup> A =  $\text{Na}_2\text{CO}_3 \cdot 10\text{H}_2\text{O}$ ; B =  $\text{Na}_2\text{CO}_3 \cdot \text{H}_2\text{O}$ ; C =  $\text{NaIO}_3 \cdot 5\text{H}_2\text{O}$ ; D =  $\text{NaIO}_3 \cdot \text{H}_2\text{O}$

<sup>b</sup> For the binary system the compiler computes the following:

soly of  $\text{NaIO}_3$  =  $0.125 \text{ mol kg}^{-1}$  at  $0^\circ\text{C}$   
 =  $0.479 \text{ mol kg}^{-1}$  at  $25^\circ\text{C}$   
 =  $0.6702 \text{ mol kg}^{-1}$  at  $40^\circ\text{C}$   
 =  $0.8267 \text{ mol kg}^{-1}$  at  $50^\circ\text{C}$

## COMMENTS AND/OR ADDITIONAL DATA:

The phase diagram is given below (based on mass % units).



System  $\text{NaIO}_3\text{-Na}_2\text{CO}_3\text{-H}_2\text{O}$ , showing the solubility isotherms at four temperatures, and the stability areas of the five solid phases. No double salt exists.

|   |                   |                     |   |                     |  |
|---|-------------------|---------------------|---|---------------------|--|
| <b>COMPONENTS:</b><br>(1) Sodium nitrate; $\text{NaNO}_3$ ; [7631-99-4]<br>(2) Sodium iodate; $\text{NaIO}_3$ ; [7681-55-2]<br>(3) Water; $\text{H}_2\text{O}$ ; [7732-18-5]  |                   |                     | <b>ORIGINAL MEASUREMENTS:</b><br>Foote, H.W.; Vance, J.E.<br><i>Am. J. Sci.</i> <u>1929</u> , <i>18</i> , 375-82.           |                     |  |
| <b>VARIABLES:</b><br>Composition<br>T/K = 273 - 308   |                   |                     | <b>PREPARED BY:</b><br>Hiroshi Miyamoto   |                     |  |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions  |                   |                     |   |                     |  |
| t/°C  | $\text{NaIO}_3$   |                     | $\text{NaNO}_3$   |                     | Nature of the solid phase <sup>a</sup> |
|   | mass %            | mol %<br>(compiler) | mass %  | mol %<br>(compiler) |  |
| 0   | -                 | -                   | 42.13   | 13.37               | A                                      |
|   | 0.82              | 0.113               | 41.76   | 13.34               | A+D                                    |
|   | 0.82              | 0.112               | 41.71   | 13.32               | "                                      |
|   | 0.86              | 0.117               | 41.15   | 13.06               | D                                      |
|   | 1.00              | 0.131               | 37.53   | 11.44               | "                                      |
|   | 1.16              | 0.147               | 34.61   | 10.24               | "                                      |
|   | 1.31              | 0.163               | 32.57   | 9.438               | "                                      |
|   | 1.38              | 0.171               | 32.19   | 9.298               | B+D                                    |
|   | 1.31              | 0.163               | 32.45   | 9.391               | "                                      |
|   | 1.26              | 0.151               | 29.18   | 8.153               | B                                      |
|   | 1.06              | 0.117               | 21.42   | 5.526               | "                                      |
|   | 2.42 <sup>b</sup> | 0.225               | -   | -                   | "                                      |
| 8   | -                 | -                   | 43.99   | 14.27               | A                                      |
|   | 1.67              | 0.236               | 43.28   | 14.25               | A+D                                    |
|   | 1.67              | 0.236               | 43.21   | 14.21               | "                                      |
|   | 1.88              | 0.259               | 40.80   | 13.08               | D                                      |
|   | 1.96              | 0.266               | 39.54   | 12.50               | C+D                                    |
|   | 2.02              | 0.274               | 39.36   | 12.42               | C                                      |
|   | 2.27              | 0.285               | 32.23   | 9.418               | "                                      |
| continued.....  |                   |                     |   |                     |  |
| <b>AUXILIARY INFORMATION</b>  |                   |                     |   |                     |  |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Sodium iodate, sodium nitrate and water were placed in glass stoppered bottles and rotated in a thermostat. Samples of the solution were drawn off through glass wool filters. The iodate content was determined by adding KI to the solution, acidifying with sulfuric acid, and titrating the free iodine with sodium thiosulfate solution. The nitrate content was calculated from the iodate concentration and the total mass of salts in solution. Water was found by difference. The solid phases were analyzed as wet residues after largely freeing them from water by pressing between filter papers. The composition of the dry residue was determined by Schreinemakers' method. |                   |                     | <b>SOURCE AND PURITY OF MATERIALS:</b><br>Sodium iodate and nitrate used were c.p. products which were recrystallized once. |                     |  |
|   |                   |                     | <b>ESTIMATED ERROR:</b><br>Nothing specified.   |                     |  |
|   |                   |                     | <b>REFERENCES:</b>  |                     |  |

|  |   |
|--|---|
| <b>COMPONENTS:</b><br>(1) Sodium nitrate; $\text{NaNO}_3$ ; [7631-99-4]<br>(2) Sodium iodate; $\text{NaIO}_3$ ; [7681-55-2]<br>(3) Water; $\text{H}_2\text{O}$ ; [7732-18-5] | <b>ORIGINAL MEASUREMENTS:</b><br>Foote, H.W.; Vance, J.E.<br><i>Am. J. Sci.</i> <u>1929</u> , 18, 375-82. |
|--|---|

**EXPERIMENTAL VALUES: (Continued)**

## Composition of saturated solutions

| t/°C               | $\text{NaIO}_3$   |                     | $\text{NaNO}_3$ |                     | Nature of the solid phase <sup>a</sup> |
|--------------------|-------------------|---------------------|-----------------|---------------------|--|
|                    | mass %            | mol %<br>(compiler) | mass %          | mol %<br>(compiler) |  |
| 8                  | 2.25              | 0.279               | 31.03           | 8.948               | B+C                                    |
|                    | 2.22              | 0.274               | 30.83           | 8.868               | "                                      |
|                    | 3.90 <sup>b</sup> | 0.368               | -               | -                   | B                                      |
| 25                 | -                 | -                   | 48.04           | 16.39               | A                                      |
|                    | 1.09              | 0.161               | 47.39           | 16.29               | "                                      |
|                    | 2.30              | 0.343               | 46.73           | 16.21               | A+C                                    |
|                    | 2.25              | 0.335               | 46.65           | 16.16               | "                                      |
|                    | 2.38              | 0.340               | 43.18           | 14.34               | C                                      |
|                    | 2.55              | 0.350               | 39.88           | 12.76               | "                                      |
|                    | 3.69              | 0.400               | 15.94           | 4.018               | "                                      |
| 8.66 <sup>b</sup>  | 0.856             | -                   | -               | "                   |  |
| 35                 | -                 | -                   | 50.15           | 17.58               | A                                      |
|                    | 1.58              | 0.241               | 49.25           | 17.47               | "                                      |
|                    | 2.55              | 0.391               | 48.68           | 17.39               | A+C                                    |
|                    | 2.55              | 0.391               | 48.68           | 17.39               | "                                      |
|                    | 2.60              | 0.399               | 48.68           | 17.41               | "                                      |
|                    | 2.66              | 0.400               | 46.99           | 16.45               | C                                      |
|                    | 3.85              | 0.456               | 24.96           | 6.886               | "                                      |
| 10.57 <sup>b</sup> | 1.065             | -                   | -               | "                   |  |

<sup>a</sup> A =  $\text{NaNO}_3$ ; B =  $\text{NaIO}_3 \cdot 5\text{H}_2\text{O}$ ; C =  $\text{NaIO}_3 \cdot \text{H}_2\text{O}$ ; D =  $2\text{NaIO}_3 \cdot 3\text{NaNO}_3 \cdot 15\text{H}_2\text{O}$

<sup>b</sup> For the binary system the compiler computes the following:

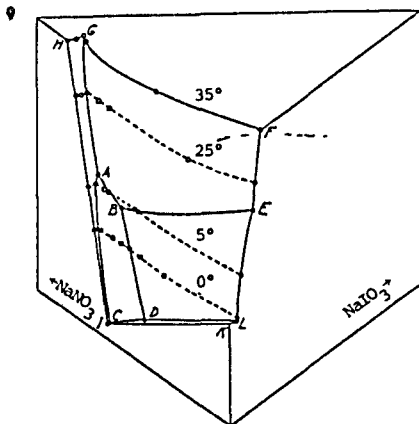
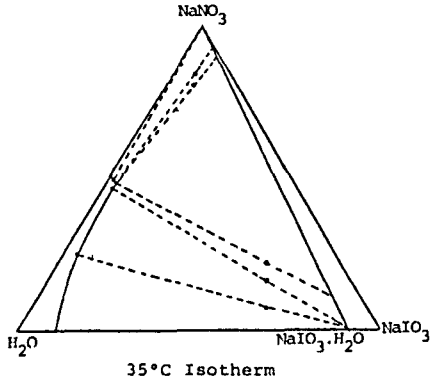
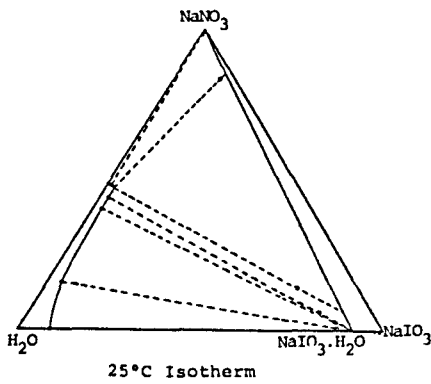
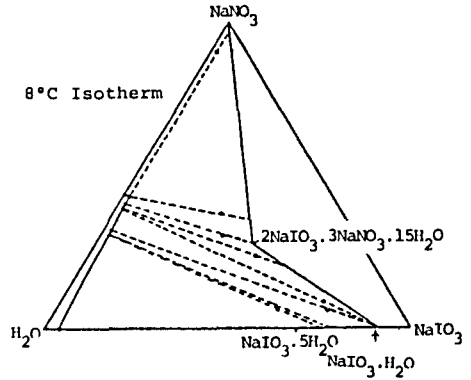
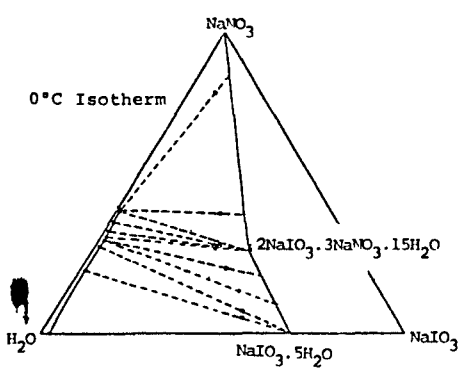
soly of  $\text{NaIO}_3$  = 0.125 mol  $\text{kg}^{-1}$  at 0°C; = 0.205 mol  $\text{kg}^{-1}$  at 8°C  
 = 0.479 mol  $\text{kg}^{-1}$  at 25°C; = 0.5973 mol  $\text{kg}^{-1}$  at 35°C

**COMMENTS AND/OR ADDITIONAL DATA:**

Isotherms based on mass % units are reproduced below on the following page.

|  |   |
|--|---|
| <p>COMPONENTS:</p> <p>(1) Sodium nitrate; <math>\text{NaNO}_3</math>; [7631-99-4]</p> <p>(2) Sodium iodate; <math>\text{NaIO}_3</math>; [7681-55-2]</p> <p>(3) Water; <math>\text{H}_2\text{O}</math>; [7732-18-5]</p> | <p>ORIGINAL MEASUREMENTS:</p> <p>Foote, H.W.; Vance, J.E.</p> <p><i>Am. J. Sci.</i> 1929, 18, 375-82.</p> |
|--|---|

COMMENTS AND/OR ADDITIONAL DATA: (Continued)



| EXPERIMENTAL VALUES: |               |                                    |                      | Composition of saturated solutions |                                    |                      |                               |   |
|----------------------|---------------|------------------------------------|----------------------|------------------------------------|------------------------------------|----------------------|-------------------------------|---|
| t/°C                 | Sodium iodate |                                    |                      | Sodium nitrate                     |                                    |                      | Density<br>g cm <sup>-3</sup> | Nature of the<br>solid phase <sup>a</sup> |
|                      | mass %        | g <sub>2</sub> /100 g <sub>3</sub> | mol kg <sup>-1</sup> | mass %                             | g <sub>1</sub> /100 g <sub>3</sub> | mol kg <sup>-1</sup> |                               |   |
| 0                    | 0.53          | 0.92                               | 0.046                | 42.0                               | 72.9                               | 8.58                 | 1.357                         | A   |
|                      | 0.82          | 1.43                               | 0.0723               | 41.9                               | 73.0                               | 8.59                 | 1.360                         | A+S                                       |
|                      | 0.85          | 1.46                               | 0.0738               | 40.8                               | 69.9                               | 8.22                 | 1.351                         | S   |
|                      | 1.25          | 1.92                               | 0.0970               | 33.5                               | 51.3                               | 6.04                 | 1.286                         | "   |
|                      | 1.34          | 2.02                               | 0.102                | 32.5                               | 49.1                               | 5.78                 | 1.278                         | S+B                                       |
|                      | 1.25          | 1.81                               | 0.0915               | 29.6                               | 42.8                               | 5.04                 | 1.251                         | B   |
| 5                    | 1.28          | 2.28                               | 0.115                | 42.8                               | 76.4                               | 8.99                 | 1.373                         | A+S                                       |
|                      | 2.02          | 3.15                               | 0.159                | 34.1                               | 53.4                               | 6.28                 | 1.300                         | B+C+S                                     |
| 10 <sup>m</sup>      | 2.04          |                                    |                      |                                    |                                    |                      | 1.388                         | A+S                                       |
| 9.7 <sup>i</sup>     | 1.97          | 3.57                               | 0.180                | 43.5                               | 79.6                               | 9.37                 | 1.387                         | A+C+S                                     |
| 10                   | 1.98          | 3.64                               | 0.184                | 43.6                               | 80.1                               | 9.42                 | 1.388                         | A+C                                       |
| 15 <sup>i</sup>      | 2.95          | 3.63                               | 0.183                | 15.8                               | 19.5                               | 2.29                 | 1.144                         | B+C                                       |
| 20                   | 2.14          | 4.11                               | 0.208                | 45.7                               | 87.6                               | 10.3                 | 1.405                         | A+C                                       |
| 30                   | 2.43          | 4.88                               | 0.247                | 47.8                               | 95.8                               | 11.3                 | 1.423                         | "   |
| 35                   | 2.58          |                                    |                      |                                    |                                    |                      | 1.432                         | "   |
| 40                   | 2.77          | 5.83                               | 0.295                | 49.7                               | 104.7                              | 12.32                | 1.442                         | "   |
| 50                   | 3.24          |                                    |                      |                                    |                                    |                      | 1.462                         | "   |

continued....

## AUXILIARY INFORMATION

## METHOD/APPARATUS/PROCEDURE:

The details of procedure were not given. The iodate content was determined by titration with thiosulfate solution. The total solids were determined by evaporation of the solution at about 140°C. The compiler assumes that the concentration of the nitrate was determined by difference.

## SOURCE AND PURITY OF MATERIALS:

Sodium iodate used was purchased as a "pure chemical". The salt was recrystallized four times. The product obtained was the monohydrate.

## ESTIMATED ERROR:

Nothing specified.

## REFERENCES:

| COMPONENTS:   |               |                              |                      | ORIGINAL MEASUREMENTS:                         |                              |                      |                    |               |
|---|---------------|------------------------------|----------------------|--|------------------------------|----------------------|--------------------|---------------|
| (1) Sodium nitrate; $\text{NaNO}_3$ ; [7631-99-4]   |               |                              |                      | Cornec, M.E.; Spack, A.                        |                              |                      |                    |               |
| (2) Sodium iodate; $\text{NaIO}_3$ ; [7681-55-2]  |               |                              |                      | Bull. Soc. Chim. Fr. <u>1931</u> , 49, 582-94. |                              |                      |                    |               |
| (3) Water; $\text{H}_2\text{O}$ ; [7732-18-5]   |               |                              |                      |  |                              |                      |                    |               |
| EXPERIMENTAL VALUES: (Continued)  |               |                              |                      |  |                              |                      |                    |               |
| Composition of saturated solutions  |               |                              |                      |  |                              |                      |                    |               |
| $t/^\circ\text{C}$  | Sodium iodate |                              |                      | Sodium nitrate                                 |                              |                      | Density            | Nature of the |
|   | mass %        | $\text{g}_2/100 \text{ g}_3$ | $\text{mol kg}^{-1}$ | mass %   | $\text{g}_1/100 \text{ g}_3$ | $\text{mol kg}^{-1}$ | $\text{g cm}^{-3}$ | solid phase   |
| 41.5 <sup>i</sup>   | 2.85          | 6.0                          | 0.30                 | 50.0   | 106.0                        | 12.47                | 1.445              | A+C+D         |
| 35 <sup>m</sup>   | 2.85          |                              |                      |  |                              |                      | 1.435              | A+D           |
| 50  | 2.90          | 6.39                         | 0.323                | 51.7   | 114.1                        | 13.42                | 1.458              | "             |
| 60  | 2.97          | 6.87                         | 0.347                | 53.8   | 124.4                        | 14.64                | 1.474              | "             |
| 70  | 3.16          | 7.68                         | 0.388                | 55.7   | 135.3                        | 15.92                | 1.491              | "             |
| 80  | 3.35          | 8.60                         | 0.435                | 57.7   | 148.2                        | 17.44                | 1.509              | "             |
| 90  | 3.60          | 9.79                         | 0.495                | 59.6   | 162.3                        | 19.10                | 1.528              | "             |
| 100   | 3.94          | 11.40                        | 0.5761               | 61.5   | 177.9                        | 20.93                | 1.549              | "             |
| 15  | 3.05          | 3.49                         | 0.176                | 9.4  | 10.8                         | 1.27                 | 1.096              | B             |
| 15  | 2.97          | 3.50                         | 0.177                | 12.2   | 14.4                         | 1.69                 | 1.116              | "             |
| 15  | 2.95          | 3.60                         | 0.182                | 15.0   | 18.3                         | 2.15                 | 1.138              | "             |
| 15 <sup>m</sup>   | 3.04          | 3.89                         | 0.197                | 18.8   | 24.1                         | 2.84                 | 1.170              | "             |
| 15  | 2.85          | 3.62                         | 0.183                | 18.4   | 23.3                         | 2.74                 | 1.164              | C             |
| 15 <sup>m</sup>   | 3.03          | 3.66                         | 0.185                | 14.3   | 17.2                         | 2.02                 | 1.133              | "             |
| 15 <sup>m</sup>   | 3.48          | 3.97                         | 0.201                | 8.8  | 10.1                         | 1.19                 | 1.096              | "             |
| <sup>a</sup> A = $\text{NaNO}_3$ ; B = $\text{NaIO}_3 \cdot 5\text{H}_2\text{O}$ ; C = $\text{NaIO}_3 \cdot \text{H}_2\text{O}$ ; D = $\text{NaIO}_3$ |               |                              |                      |  |                              |                      |                    |               |
| S = double salt: $2\text{NaIO}_3 \cdot 3\text{NaNO}_3 \cdot 15\text{H}_2\text{O}$ .   |               |                              |                      |  |                              |                      |                    |               |
| <sup>m</sup> Metastable   |               |                              |                      |  |                              |                      |                    |               |
| <sup>i</sup> Interpolated.  |               |                              |                      |  |                              |                      |                    |               |



|  |                  |  |        |   |                               |   |  |
|--|------------------|--|--------|---|-------------------------------|---|--|
| <b>COMPONENTS:</b><br>(1) Sodium nitrate; $\text{NaNO}_3$ ; [7631-99-4]<br>(2) Sodium iodate; $\text{NaIO}_3$ ; [7681-55-2]<br>(3) Water; $\text{H}_2\text{O}$ ; [7732-18-5]   |                  |  |        | <b>ORIGINAL MEASUREMENTS:</b><br>Hill, A.E.; Donovan, J.E.<br><br><i>J. Am. Chem. Soc.</i> <u>1931</u> , 53, 934-41.                  |                               |   |  |
| <b>VARIABLES:</b><br>Composition<br>T/K = 278.15 - 313.15  |                  |  |        | <b>PREPARED BY:</b><br>Hiroshi Miyamoto   |                               |   |  |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions   |                  |  |        |   |                               |   |  |
| $t/^\circ\text{C}$   | mass %           | $\text{NaIO}_3$<br>mol %<br>(compiler) | mass % | $\text{NaNO}_3$<br>mol %<br>(compiler)  | Density<br>$\text{g cm}^{-3}$ | Nature of the<br>solid phase <sup>a</sup> |  |
| 5  | 3.3 <sup>b</sup> | 0.310                                  | 0.00   | 0.00  | 1.028                         | A   |  |
|  | 1.58             | 0.151                                  | 4.50   | 1.00  | 1.042                         | "   |  |
|  | 1.55             | 0.175                                  | 22.59  | 5.927   | 1.182                         | "   |  |
|  | 1.65             | 0.193                                  | 26.38  | 7.195   | 1.214                         | "   |  |
|  | 1.75             | 0.210                                  | 28.44  | 7.932   | 1.230                         | "   |  |
|  | 1.87             | 0.230                                  | 30.70  | 8.781   | 1.255                         | "   |  |
|  | 1.78             | 0.220                                  | 31.38  | 9.030   | 1.262                         | "   |  |
|  | 2.10             | 0.261                                  | 31.54  | 9.128   | 1.263                         | "   |  |
|  | 2.07             | 0.260                                  | 32.48  | 9.493   | 1.275                         | "   |  |
|  | 1.86             | 0.233                                  | 32.37  | 9.424   | 1.269                         | "   |  |
|  | 1.94             | 0.248                                  | 34.34  | 10.23   | 1.291                         | A+E                                       |  |
|  | 1.76             | 0.231                                  | 36.69  | 11.19   | 1.308                         | E   |  |
|  | 1.60             | 0.213                                  | 38.38  | 11.91   | 1.324                         | "   |  |
|  | 1.52             | 0.204                                  | 39.17  | 12.25   | 1.331                         | "   |  |
|  | 1.41             | 0.192                                  | 40.40  | 12.80   | 1.336                         | "   |  |
|  | 1.28             | 0.179                                  | 42.74  | 13.90   | 1.359                         | E+D                                       |  |
|  | 1.01             | 0.141                                  | 42.94  | 13.95   | 1.359                         | D   |  |
|  | 0.00             | 0.000                                  | 43.42  | 13.99   | 1.368                         | "   |  |
| continued....  |                  |  |        |   |                               |   |  |
| <b>AUXILIARY INFORMATION</b>   |                  |  |        |   |                               |   |  |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>For sodium iodate-sodium nitrate-water system, weighed quantities of these salts were treated with weighed amounts of water in Pyrex test-tubes. The tubes were slowly rotated in a water-thermostat at the desired temperature for about two weeks. After the slns were allowed to settle, samples were withdrawn into a calibrated pipet fitted with a small cotton filter. One sample was weighed and evaporated in a platinum dish to constant weight at $110^\circ\text{C}$ . From this the water content of the saturated solution was determined.<br>To determine the $\text{NaIO}_3$ content, a second weighed sample was treated with KI and $\text{H}_2\text{SO}_4$ , and titrated with $\text{Na}_2\text{S}_2\text{O}_3$ . The sodium nitrate content was obtained by difference. |                  |  |        | <b>SOURCE AND PURITY OF MATERIALS:</b><br>"Good grade" sodium iodate and sodium nitrate were purified by recrystallization.           |                               |   |  |
|  |                  |  |        | <b>ESTIMATED ERROR:</b><br>Soly: the error for the analysis of iodate by iodometry was within 0.2 %.<br>Temp: precision $\pm 0.05$ K. |                               |   |  |
|  |                  |  |        | <b>REFERENCES:</b>  |                               |   |  |

| COMPONENTS:   |                             |  |                             |  | ORIGINAL MEASUREMENTS:   |   |
|---|-----------------------------|--|-----------------------------|--|--|---|
| (1) Sodium nitrate; NaNO <sub>3</sub> ; [7631-99-4]   |                             |  |                             |  | Hill, A.E.; Donovan, J.E.<br>J. Am. Chem. Soc. <u>1931</u> , 53, 934-41. |   |
| (2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]  |                             |  |                             |  |  |   |
| (3) Water; H <sub>2</sub> O; [7732-18-5]  |                             |  |                             |  |  |   |
| EXPERIMENTAL VALUES: (Continued)  |                             |  |                             |  |  |   |
| Composition of saturated solutions  |                             |  |                             |  |  |   |
| t/°C  | NaIO <sub>3</sub><br>mass % | NaIO <sub>3</sub><br>mol %<br>(compiler) | NaNO <sub>3</sub><br>mass % | NaNO <sub>3</sub><br>mol %<br>(compiler) | Density<br>g cm <sup>-3</sup>  | Nature of the<br>solid phase <sup>a</sup> |
| 25  | 8.67 <sup>b</sup>           | 0.857                                    | 0.00                        | 0.00                                     | 1.077  | B   |
|   | 6.38                        | 0.634                                    | 3.26                        | 0.754                                    | 1.078  | "   |
|   | 5.99                        | 0.596                                    | 3.91                        | 0.906                                    | 1.078  | "   |
|   | 4.80                        | 0.486                                    | 7.32                        | 1.726                                    | 1.092  | "   |
|   | 4.30                        | 0.444                                    | 10.10                       | 2.429                                    | 1.109  | "   |
|   | 3.68                        | 0.399                                    | 16.08                       | 4.058                                    | 1.149  | "   |
|   | 3.41                        | 0.381                                    | 19.47                       | 5.060                                    | 1.171  | "   |
|   | 3.06                        | 0.367                                    | 27.16                       | 7.593                                    | 1.232  | "   |
|   | 2.84                        | 0.361                                    | 32.67                       | 9.661                                    | 1.276  | "   |
|   | 2.60                        | 0.350                                    | 38.19                       | 11.98                                    | 1.328  | "   |
|   | 2.31                        | 0.337                                    | 45.12                       | 15.34                                    | 1.392  | "   |
|   | 2.23                        | 0.332                                    | 46.81                       | 16.24                                    | 1.408  | B+D                                       |
|   | 1.09                        | 0.161                                    | 47.44                       | 16.32                                    | 1.396  | D   |
|   | 0.00                        | 0.00                                     | 47.98                       | 16.35                                    | 1.388  | "   |
| 50  | 13.95 <sup>b</sup>          | 1.454                                    | 0.00                        | 0.00                                     | -  | B   |
|   | 9.63                        | 1.011                                    | 5.74                        | 1.403                                    | -  | "   |
|   | 6.22                        | 0.700                                    | 17.03                       | 4.460                                    | -  | "   |
|   | 4.82                        | 0.598                                    | 28.18                       | 8.136                                    | -  | "   |
|   | 3.92                        | 0.544                                    | 39.15                       | 12.65                                    | -  | "   |
|   | 4.00                        | 0.561                                    | 39.94                       | 13.05                                    | -  | "   |
|   | 3.84                        | 0.548                                    | 41.53                       | 13.80                                    | -  | B+C                                       |
|   | 3.77                        | 0.542                                    | 42.26                       | 14.16                                    | -  | C   |
|   | 3.64                        | 0.531                                    | 43.46                       | 14.75                                    | -  | "   |
|   | 3.46                        | 0.515                                    | 45.23                       | 15.66                                    | -  | "   |
|   | 3.09                        | 0.481                                    | 49.11                       | 17.80                                    | -  | "   |
|   | 2.91                        | 0.469                                    | 51.86                       | 19.46                                    | -  | C+D                                       |
|   | 1.58                        | 0.252                                    | 52.55                       | 19.49                                    | -  | D   |
|   | 0.00                        | 0.000                                    | 53.50                       | 19.61                                    | -  | "   |
| <sup>a</sup> A = NaIO <sub>3</sub> ·5H <sub>2</sub> O;    B = NaIO <sub>3</sub> ·H <sub>2</sub> O;    C = NaIO <sub>3</sub> ;    D = NaNO <sub>3</sub> ;<br>E = 2NaIO <sub>3</sub> ·3NaNO <sub>3</sub> ·15H <sub>2</sub> O. |                             |  |                             |  |  |   |
| <sup>b</sup> For the binary system the compiler computes the following:   |                             |  |                             |  |  |   |
| soly of NaIO <sub>3</sub> = 0.172 mol kg <sup>-1</sup> at 5°C   |                             |  |                             |  |  |   |
| = 0.480 mol kg <sup>-1</sup> at 25°C  |                             |  |                             |  |  |   |
| = 0.8192 mol kg <sup>-1</sup> at 50°C   |                             |  |                             |  |  |   |
| continued....   |                             |  |                             |  |  |   |

## COMPONENTS:

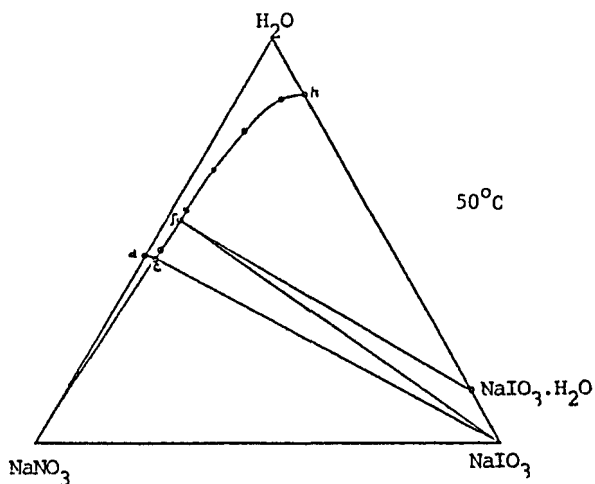
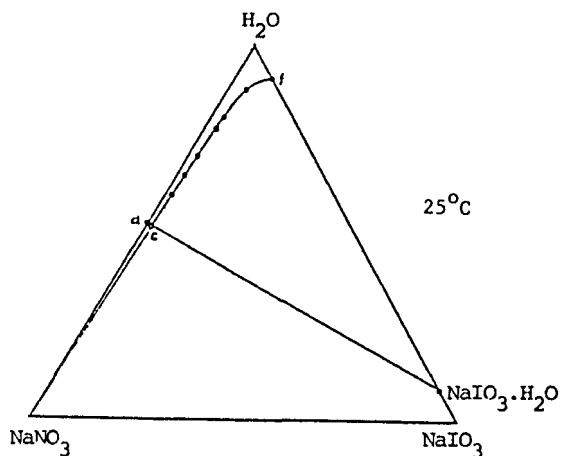
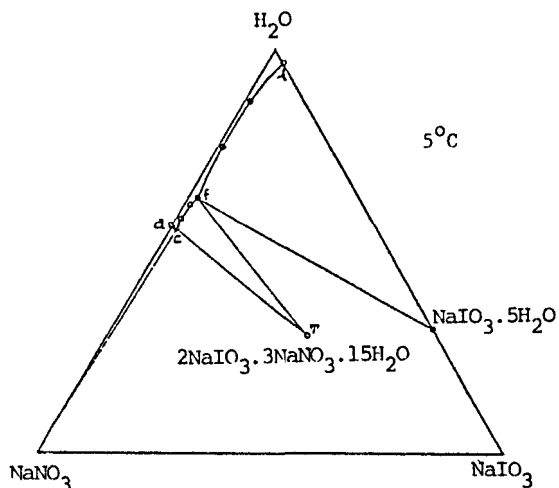
- (1) Sodium nitrate;  $\text{NaNO}_3$ ; [7631-99-4]  
 (2) Sodium iodate;  $\text{NaIO}_3$ ; [7681-55-2]  
 (3) Water;  $\text{H}_2\text{O}$ ; [7732-18-5]

## ORIGINAL MEASUREMENTS:

Hill, A.E.; Donovan, J.E.  
*J. Am. Chem. Soc.* 1931, 53, 934-41.

## COMMENTS AND/OR ADDITIONAL DATA:

Isotherms based on mass % units are reproduced below.



|  |                   |  |   |  |   |
|--|-------------------|--|---|--|---|
| <b>COMPONENTS:</b><br>(1) Sodium sulfate; Na <sub>2</sub> SO <sub>4</sub> ; [7757-82-6]<br>(2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]<br>(3) Water; H <sub>2</sub> O; [7732-18-5]  |                   |  | <b>ORIGINAL MEASUREMENTS:</b><br>Foote, H.W.; Vance, J.E.<br><i>Am. J. Sci.</i> <u>1930</u> , 19, 203-13.                                   |  |   |
| <b>VARIABLES:</b><br>Composition<br>T/K = 298 - 323  |                   |  | <b>PREPARED BY:</b><br>Hiroshi Miyamoto   |  |   |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions   |                   |  |   |  |   |
| t/°C   | mass %            | NaIO <sub>3</sub><br>mol %<br>(compiler) | mass %  | Na <sub>2</sub> SO <sub>4</sub><br>mol %<br>(compiler) | Nature of the<br>solid phase <sup>b</sup> |
| 25   | -                 | -  | 21.75   | 3.405  | A   |
|  | 2.20              | 0.252                                    | 21.30   | 3.402  | "   |
|  | 2.80              | 0.323                                    | 21.18   | 3.402  | A+C                                       |
|  | 2.78              | 0.320                                    | 21.18   | 3.401  | "   |
|  | 2.80              | 0.323                                    | 21.19   | 3.404  | "   |
|  | 3.17              | 0.353                                    | 17.52   | 2.716  | C   |
|  | 3.76              | 0.400                                    | 12.64   | 1.874  | "   |
|  | 8.66 <sup>c</sup> | 0.856                                    | -   | -  | "   |
| 29.5   | -                 | -  | 28.12   | 4.727  | A   |
|  | 1.62              | 0.198                                    | 27.72   | 4.730  | A+E                                       |
|  | 1.53              | 0.187                                    | 27.72   | 4.725  | "   |
|  | 1.52              | 0.184                                    | 26.85   | 4.530  | E   |
|  | 1.90              | 0.228                                    | 25.68   | 4.294  | "   |
|  | 2.70              | 0.325                                    | 25.17   | 4.225  | C+E                                       |
|  | 2.73              | 0.328                                    | 24.86   | 4.159  | "   |
|  | 9.47 <sup>c</sup> | 0.943                                    | -   | -  | C   |
| 35   | -                 | -  | 33.10   | 5.905  | B   |
|  | (A) 0.15          | 0.019                                    | 32.86   | 5.856  | B+D                                       |
|  | 0.15              | 0.019                                    | 32.91   | 5.868  | "   |
| continued.....   |                   |  |   |  |   |
| <b>AUXILIARY INFORMATION</b>   |                   |  |   |  |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Sodium iodate, sodium sulfate and water were placed in glass stoppered bottles and the bottles rotated in a thermostat. Two weeks were allowed for the attainment of equilibrium except in the case of the solubility isotherm at 25°C and 50°C where a minimum of 48 hours were allowed. Samples of the solution were drawn off through glass wool filters for analysis. The composition of the dry solid phases were determined by the method of Schreinemakers'. Sodium iodate in the liquid and solid phases was determined by adding potassium iodide to the samples, acidifying with sulfuric acid, and titrating the liberated iodine with thiosulfate solution. The sulfate content was calculated from the iodate concentration and the mass of total salts. Water was found by difference. |                   |  | <b>SOURCE AND PURITY OF MATERIALS:</b><br>The authors only stated that sodium iodate and sodium sulfate were purified by customary methods. |  |   |
|  |                   |  | <b>ESTIMATED ERROR:</b><br>Nothing specified.   |  |   |
|  |                   |  | <b>REFERENCES:</b>  |  |   |

|  |  |
|--|--|
| COMPONENTS:<br>(1) Sodium sulfate; $\text{Na}_2\text{SO}_4$ ; [7757-82-6]<br>(2) Sodium iodate; $\text{NaIO}_3$ ; [7681-55-2]<br>(3) Water; $\text{H}_2\text{O}$ ; [7732-18-5] | ORIGINAL MEASUREMENTS:<br>Foote, H.W.; Vance, J.E.<br><i>Am. J. Sci.</i> <u>1930</u> , 19, 203-13. |
|--|--|

## EXPERIMENTAL VALUES; (Continued)

## Composition of saturated solutions

| t/°C | $\text{NaIO}_3$      |                     | $\text{Na}_2\text{SO}_4$ |                     | Nature of the solid phase <sup>b</sup> |
|------|----------------------|---------------------|--------------------------|---------------------|--|
|      | mass %               | mol %<br>(compiler) | mass %                   | mol %<br>(compiler) |  |
| 35   |                      |                     |                          |                     |  |
| (A)  | 0.11                 | 0.014               | 32.83                    | 5.845               | D                                      |
|      | 0.16                 | 0.020               | 32.18                    | 5.688               | "                                      |
|      | 0.29                 | 0.036               | 30.92                    | 5.392               | "                                      |
|      | 0.57                 | 0.070               | 29.63                    | 5.105               | "                                      |
|      | 0.62                 | 0.076               | 28.98                    | 4.958               | D+E                                    |
|      | 0.80                 | 0.098               | 28.77                    | 4.921               | "                                      |
|      | 1.30                 | 0.156               | 26.06                    | 4.345               | E                                      |
|      | 2.34                 | 0.276               | 23.62                    | 3.878               | "                                      |
|      | 3.33                 | 0.392               | 22.57                    | 3.705               | C+E                                    |
|      | 3.59                 | 0.415               | 20.70                    | 3.338               | C                                      |
|      | 3.73                 | 0.426               | 19.33                    | 3.075               | "                                      |
|      | 4.47                 | 0.493               | 15.30                    | 2.350               | "                                      |
|      | 10.57 <sup>c</sup>   | 1.065               | -                        | -                   | "                                      |
| 35   |                      |                     |                          |                     |  |
| (B)  | -                    | -                   | 33.10 <sup>a</sup>       | 5.905               | B                                      |
|      | 0.15 <sup>a</sup>    | 0.019               | 32.86                    | 5.856               | B+D                                    |
|      | 0.15 <sup>a</sup>    | 0.019               | 32.91                    | 5.868               | "                                      |
|      | 0.10                 | 0.013               | 32.82                    | 5.842               | D                                      |
|      | 0.28                 | 0.035               | 31.06                    | 5.424               | "                                      |
|      | 0.30                 | 0.037               | 30.35                    | 5.257               | "                                      |
|      | 0.83                 | 0.102               | 28.84                    | 4.939               | D+E                                    |
|      | 0.90                 | 0.110               | 28.50                    | 4.864               | "                                      |
|      | 1.29                 | 0.154               | 25.97                    | 4.325               | E                                      |
|      | 2.39                 | 0.282               | 23.79                    | 3.916               | "                                      |
|      | 3.33 <sup>a</sup>    | 0.392               | 22.57                    | 3.705               | C+E                                    |
|      | 3.59 <sup>a</sup>    | 0.415               | 20.70                    | 3.338               | C                                      |
|      | 3.73 <sup>a</sup>    | 0.426               | 19.33                    | 3.075               | "                                      |
|      | 4.47 <sup>a</sup>    | 0.493               | 15.30                    | 2.350               | "                                      |
|      | 10.57 <sup>a,c</sup> | 1.065               | -                        | -                   | "                                      |

<sup>a</sup> Data taken from 35(A) isotherm

|    |                    |       |       |       |     |
|----|--------------------|-------|-------|-------|-----|
| 50 | -                  | -     | 31.76 | 5.574 | B   |
|    | 0.17               | 0.21  | 31.60 | 5.547 | B+D |
|    | 0.13               | 0.016 | 31.70 | 5.569 | "   |
|    | 0.15               | 0.019 | 31.67 | 5.563 | D   |
|    | 0.28               | 0.035 | 30.02 | 5.178 | "   |
|    | 0.63               | 0.077 | 28.53 | 4.856 | "   |
|    | 0.98               | 0.119 | 27.56 | 4.658 | D+E |
|    | 1.06               | 0.128 | 27.28 | 4.600 | "   |
|    | 1.25               | 0.149 | 25.93 | 4.315 | E   |
|    | 1.87               | 0.220 | 23.96 | 3.927 | "   |
|    | 2.75               | 0.323 | 22.85 | 3.737 | "   |
|    | 4.01               | 0.469 | 21.21 | 3.456 | "   |
|    | 5.29               | 0.619 | 19.97 | 3.258 | C+E |
|    | 5.32               | 0.623 | 19.97 | 3.259 | "   |
|    | 14.06 <sup>c</sup> | 1.468 | -     | -     | C   |

continued.....

## COMPONENTS:

- (1) Sodium sulfate;  $\text{Na}_2\text{SO}_4$ ; [7757-82-6]  
 (2) Sodium iodate;  $\text{NaIO}_3$ ; [7681-55-2]  
 (3) Water;  $\text{H}_2\text{O}$ ; [7732-18-5]

## ORIGINAL MEASUREMENTS:

Foote, H.W.; Vance, J.E.  
*Am. J. Sci.* 1930, 19, 203-13.

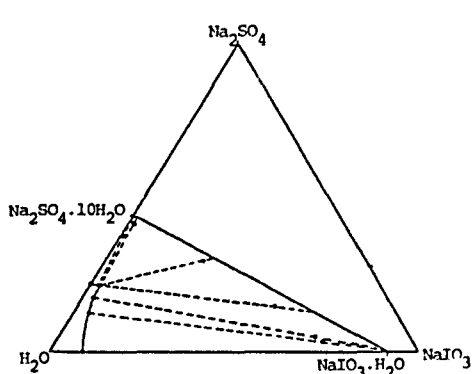
## EXPERIMENTAL VALUES: (Continued)

- <sup>b</sup> A =  $\text{Na}_2\text{SO}_4 \cdot 10\text{H}_2\text{O}$ ; B =  $\text{Na}_2\text{SO}_4$ ; C =  $\text{NaIO}_3 \cdot \text{H}_2\text{O}$ ; D =  $\text{NaIO}_3 \cdot 4\text{Na}_2\text{SO}_4$ ;  
 E =  $\text{NaIO}_3 \cdot 3\text{Na}_2\text{SO}_4$

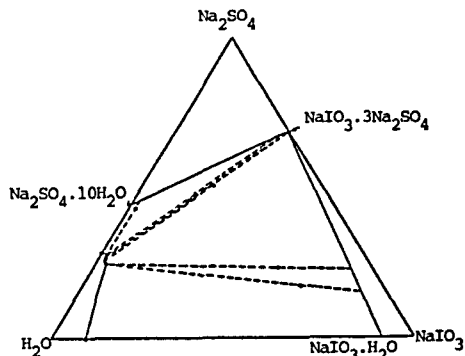
- <sup>c</sup> For the binary system the compiler computes the following:  
 soly of  $\text{NaIO}_3$  = 0.479 mol  $\text{kg}^{-1}$  at 25°C; 0.529 mol  $\text{kg}^{-1}$  at 29.5°C  
 0.5973 mol  $\text{kg}^{-1}$  at 35°C; 0.8267 mol  $\text{kg}^{-1}$  at 50°C

## COMMENTS AND/OR ADDITIONAL DATA:

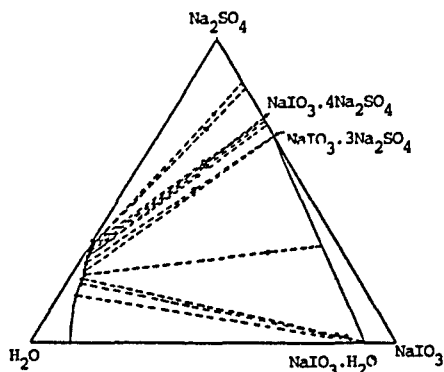
The solubility isotherms are reported below (based on mass % units)



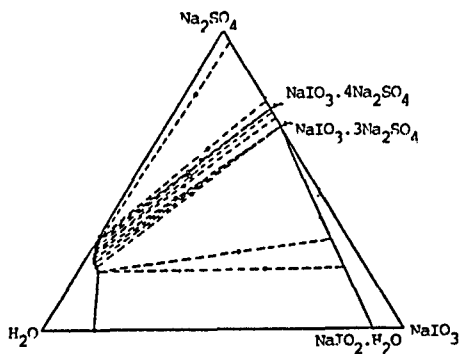
25°C Isotherm



29.5°C Isotherm



35°C Isotherm



50°C Isotherm

|   |                   |                     |  |                     |  |
|---|-------------------|---------------------|--|---------------------|--|
| <b>COMPONENTS:</b>  |                   |                     | <b>ORIGINAL MEASUREMENTS:</b>  |                     |  |
| (1) Sodium chloride; NaCl; [7647-14-5]  |                   |                     | Foote, H.W.; Vance, J.E.   |                     |  |
| (2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]  |                   |                     | Am. J. Sci. <u>1929</u> , 17, 425-30.  |                     |  |
| (3) Water; H <sub>2</sub> O; [7732-18-5]  |                   |                     |  |                     |  |
| <b>VARIABLES:</b>   |                   |                     | <b>PREPARED BY:</b>  |                     |  |
| Composition at 273, 288, 298 and 308 K  |                   |                     | Hiroshi Miyamoto   |                     |  |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions  |                   |                     |  |                     |  |
| t/°C  | NaIO <sub>3</sub> |                     | NaCl   |                     | Nature of the solid phase <sup>a</sup> |
|   | mass %            | mol %<br>(compiler) | mass %   | mol %<br>(compiler) |  |
| 0   | -                 | -                   | 26.34  | 9.928               | A                                      |
|   | 0.29              | 0.032               | 26.36  | 9.970               | A+D                                    |
|   | 0.37              | 0.041               | 26.28  | 9.942               | "                                      |
|   | 0.38              | 0.042               | 26.30  | 9.952               | "                                      |
|   | 0.54              | 0.059               | 24.16  | 8.995               | D                                      |
|   | 0.66              | 0.072               | 23.08  | 8.527               | "                                      |
|   | 0.73              | 0.079               | 22.62  | 8.332               | "                                      |
|   | 1.03              | 0.111               | 20.85  | 7.593               | D+B                                    |
|   | 1.03              | 0.111               | 20.88  | 7.606               | "                                      |
|   | 0.83              | 0.086               | 16.30  | 5.712               | B                                      |
|   | 2.42 <sup>b</sup> | 0.225               | -  | -                   | "                                      |
| 15  | -                 | -                   | 26.38  | 9.947               | A                                      |
|   | 0.97              | 0.109               | 26.14  | 9.943               | A+D                                    |
|   | 0.97              | 0.109               | 26.12  | 9.934               | "                                      |
|   | 0.97              | 0.109               | 26.30  | 10.02               | "                                      |
|   | 1.29              | 0.144               | 24.64  | 9.287               | D                                      |
|   | 1.68              | 0.185               | 23.14  | 8.650               | C+D                                    |
|   | 1.71              | 0.189               | 23.14  | 8.653               | "                                      |
|   | 1.75              | 0.190               | 20.73  | 7.601               | C                                      |
|   | 1.87              | 0.196               | 16.32  | 5.782               | "                                      |
| continued.....  |                   |                     |  |                     |  |
| <b>AUXILIARY INFORMATION</b>  |                   |                     |  |                     |  |
| <b>METHOD/APPARATUS/PROCEDURE:</b>  |                   |                     | <b>SOURCE AND PURITY OF MATERIALS:</b>   |                     |  |
| Sodium iodate, sodium chloride and water were placed in glass stoppered bottles, and the bottles rotated in a thermostat for 24 hours. Samples of the solution were drawn off through glass wool filters. The iodate content was determined by adding KI to the solution, acidifying with sulfuric acid, and titrating the free iodine with sodium thio-sulfate solution. The chloride content was calculated from the IO <sub>3</sub> concentration and the total weight of salt in solution. Water was found by difference. |                   |                     | The source of NaCl and NaIO <sub>3</sub> was not given in the original paper. The authors state that the salts were purified by usual methods, however, the details of purification were not reported. |                     |  |
| The solid phases were analyzed as wet residues after largely freeing them from water by pressing between filter papers. The composition of the dry residue was then determined by Schreinemakers' method.   |                   |                     | <b>ESTIMATED ERROR:</b>  |                     |  |
|   |                   |                     | Nothing specified.   |                     |  |
|   |                   |                     | <b>REFERENCES:</b>   |                     |  |
|   |                   |                     |  |                     |  |

|  |   |
|--|---|
| <b>COMPONENTS:</b><br>(1) Sodium chloride; NaCl; [7647-14-5]<br>(2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]<br>(3) Water; H <sub>2</sub> O; [7732-18-5] | <b>ORIGINAL MEASUREMENTS:</b><br>Foote, H.W.; Vance, J.E.<br><i>Am. J. Sci.</i> 1929, 17, 425-30. |
|--|---|

**EXPERIMENTAL VALUES: (Continued)**

| t/°C | NaIO <sub>3</sub>  |                     | NaCl   |                     | solid phase <sup>a</sup> |
|------|--------------------|---------------------|--------|---------------------|--------------------------|
|      | mass %             | mol %<br>(compiler) | mass % | mol %<br>(compiler) |                          |
| 15   | 2.34               | 0.233               | 9.46   | 3.193               | B+C                      |
|      | 2.35               | 0.234               | 9.47   | 3.197               | "                        |
|      | 2.53               | 0.247               | 6.60   | 2.184               | B                        |
|      | 5.88 <sup>b</sup>  | 0.566               | -      | -                   | "                        |
| 25   | -                  | -                   | 26.50  | 10.00               | A                        |
|      | 1.96               | 0.225               | 26.08  | 10.03               | A+C                      |
|      | 1.99               | 0.226               | 25.93  | 9.960               | "                        |
|      | 1.98               | 0.225               | 26.08  | 10.03               | "                        |
|      | 8.66 <sup>b</sup>  | 0.856               | -      | -                   | C                        |
| 35   | -                  | -                   | 26.66  | 10.08               | A                        |
|      | 1.70               | 0.193               | 26.20  | 10.05               | "                        |
|      | 2.39               | 0.273               | 26.04  | 10.06               | A+C                      |
|      | 2.40               | 0.274               | 26.00  | 10.04               | "                        |
|      | 2.39               | 0.273               | 26.02  | 10.05               | "                        |
|      | 2.41               | 0.275               | 26.07  | 10.07               | "                        |
|      | 2.47               | 0.275               | 23.15  | 8.730               | C                        |
|      | 2.57               | 0.282               | 21.24  | 7.891               | "                        |
|      | 4.51               | 0.454               | 7.87   | 2.68                | "                        |
|      | 10.57 <sup>b</sup> | 1.065               | --     | --                  | "                        |

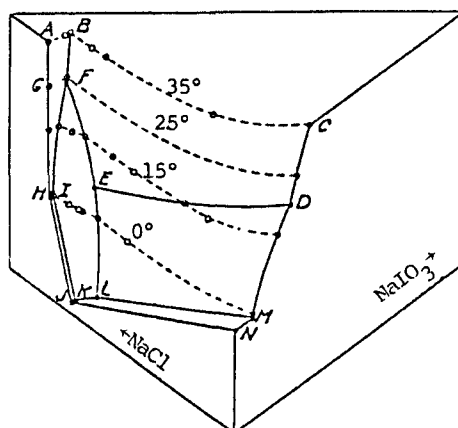
<sup>a</sup> A = NaCl; B = NaIO<sub>3</sub>·5H<sub>2</sub>O; C = NaIO<sub>3</sub>·H<sub>2</sub>O; D = 2NaIO<sub>3</sub>·3NaCl·10H<sub>2</sub>O

<sup>b</sup> For the binary system the compiler computes the following:

soly of NaIO<sub>3</sub> = 0.125 mol kg<sup>-1</sup> at 0°C  
 = 0.316 mol kg<sup>-1</sup> at 15°C  
 = 0.479 mol kg<sup>-1</sup> at 25°C  
 = 0.5973 mol kg<sup>-1</sup> at 35°C

**COMMENTS AND/OR ADDITIONAL DATA:**

The solubility isotherms are reproduced below (based on mass % units).





|   |        |       |                   |  |                    |                          |  |
|---|--------|-------|-------------------|--|--------------------|--------------------------|--|
| <b>COMPONENTS:</b>  |        |       |                   | <b>ORIGINAL MEASUREMENTS:</b>  |                    |                          |  |
| (1) Sodium bromide; NaBr; [7647-15-6]   |        |       |                   | Ricci, J.E.  |                    |                          |  |
| (2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]  |        |       |                   | J. Am. Chem. Soc. <u>1934</u> , 56, 290-5.   |                    |                          |  |
| (3) Water; H <sub>2</sub> O; [7732-18-5]  |        |       |                   |  |                    |                          |  |
| <b>VARIABLES:</b>   |        |       |                   | <b>PREPARED BY:</b>  |                    |                          |  |
| Composition   |        |       |                   | Hiroshi Miyamoto   |                    |                          |  |
| T/K = 278 - 323   |        |       |                   |  |                    |                          |  |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions  |        |       |                   |  |                    |                          |  |
| t/°C  | NaBr   |       | NaIO <sub>3</sub> |  | Density            | Nature of the            |  |
|   | mass % | mol % | mass %            | mol %  | g cm <sup>-3</sup> | solid phase <sup>a</sup> |  |
| 5   | 45.08  | 12.57 | 0.00              | 0.00   | 1.489              | A                        |  |
|   | 45.04  | 12.56 | 0.076             | 0.011  | 1.491              | A+S5                     |  |
|   | 45.00  | 12.54 | 0.075             | 0.011  | 1.492              | "                        |  |
|   | 45.07  | 12.57 | 0.073             | 0.011  | 1.492              | "                        |  |
|   | 45.04  | 12.56 | 0.075             | 0.011  | 1.492              | "                        |  |
|   | 43.99  | 12.10 | 0.084             | 0.012  | 1.473              | S5                       |  |
|   | 39.98  | 10.46 | 0.124             | 0.0169   | 1.415              | "                        |  |
|   | 35.04  | 8.655 | 0.231             | 0.0297   | 1.352              | "                        |  |
|   | 29.50  | 6.874 | 0.584             | 0.0708   | 1.287              | "                        |  |
|   | 24.56  | 5.461 | 1.09              | 0.126  | 1.238              | "                        |  |
|   | 23.53  | 5.186 | 1.27              | 0.146  | 1.229              | S5+B                     |  |
|   | 23.49  | 5.176 | 1.28              | 0.147  | 1.230              | "                        |  |
|   | 23.51  | 5.181 | 1.28              | 0.147  | 1.230              | "                        |  |
|   | 22.95  | 5.027 | 1.25              | 0.142  | 1.225              | B                        |  |
|   | 18.42  | 3.850 | 1.13              | 0.123  | 1.175              | "                        |  |
|   | 14.13  | 2.832 | 1.09              | 0.114  | 1.132              | "                        |  |
|   | 10.37  | 2.008 | 1.13              | 0.114  | 1.097              | "                        |  |
|   | 4.97   | 0.920 | 1.44              | 0.139  | 1.052              | "                        |  |
|   | 0.00   | 0.000 | 3.297             | 0.3094   | 1.027              | "                        |  |
|   | 23.30  | 5.127 | 1.34              | 0.153  | 1.227              | S5(m)                    |  |
|   | 21.71  | 4.723 | 1.78              | 0.201  | 1.215              | S5+C(m)                  |  |
|   | 20.78  | 4.476 | 1.74              | 0.195  | 1.204              | C(m)                     |  |
|   | 16.39  | 3.384 | 1.85              | 0.199  | 1.162              | "                        |  |
| continued.....  |        |       |                   |  |                    |                          |  |
| <b>AUXILIARY INFORMATION</b>  |        |       |                   |  |                    |                          |  |
| <b>METHOD/APPARATUS/PROCEDURE:</b>  |        |       |                   | <b>SOURCE AND PURITY OF MATERIALS:</b>   |                    |                          |  |
| Ternary complexes were stirred for 1-2 weeks at temperatures below 40°C, and for 2-4 days at higher temperatures (40-50°C). This length of time allowed for the attainment of equilibrium as determined in several cases by successive analysis of the solutions. Care had to be taken to seed each complex with the expected stable solid phase whenever possible, and to break up the caked hydrates which sometimes formed on mixing the salt with water in the preparation of the complexes. In one sample of the saturated solution, the iodate was determined by titration with standard thiosulfate solution. In another sample, the total solid was determined by evaporation of the solution at 100°C followed by one to two hours at 350°C. The concentration of the bromide was then determined by difference. |        |       |                   | The salts used were prepared by recrystallization of the best available c.p. material which, in the case of the bromide, usually contained from 0.5 to 1.0 % chloride. The purified salts were dried to the anhydrous state and stored at 100°C. |                    |                          |  |
|   |        |       |                   | <b>ESTIMATED ERROR:</b>  |                    |                          |  |
|   |        |       |                   | Nothing specified.   |                    |                          |  |
|   |        |       |                   | <b>REFERENCES:</b>   |                    |                          |  |
|   |        |       |                   |  |                    |                          |  |

| COMPONENTS:  |        |                     |                    | ORIGINAL MEASUREMENTS:                     |                               |   |
|--|--------|---------------------|--------------------|--|-------------------------------|---|
| (1) Sodium bromide; NaBr; [7647-15-6]              |        |                     |                    | Ricci, J.E.                                |                               |   |
| (2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2] |        |                     |                    | J. Am. Chem. Soc. <u>1934</u> , 56, 290-5. |                               |   |
| (3) Water; H <sub>2</sub> O; [7732-18-5]           |        |                     |                    |  |                               |   |
| EXPERIMENTAL VALUES: (Continued)                   |        |                     |                    |  |                               |   |
| Composition of saturated solutions                 |        |                     |                    |  |                               |   |
| t/°C   | NaBr   |                     | NaIO <sub>3</sub>  |  | Density<br>g cm <sup>-3</sup> | Nature of the<br>solid phase <sup>a</sup> |
|  | mass % | mol %<br>(compiler) | mass %             | mol %<br>(compiler)                        |                               |   |
| 5  | 12.26  | 2.438               | 2.03               | 0.210                                      | 1.123                         | C(m)                                      |
|  | 6.97   | 1.327               | 2.52               | 0.249                                      | 1.079                         | "   |
|  | 0.00   | 0.000               | 5.479 <sup>b</sup> | 0.525                                      | 1.050                         | "   |
| 15   | 46.54  | 13.23               | 0.00               | 0.000                                      | -                             | A   |
|  | 27.15  | 6.266               | 1.91               | 0.229                                      | 1.278                         | S5+C                                      |
|  | 22.08  | 4.837               | 2.05               | 0.234                                      | 1.219                         | C   |
|  | 18.54  | 3.925               | 2.20               | 0.242                                      | 1.184                         | "   |
|  | 13.41  | 2.710               | 2.53               | 0.266                                      | 1.136                         | "   |
|  | 9.16   | 1.78                | 2.69               | 0.272                                      | 1.101                         | B   |
|  | 4.27   | 0.802               | 3.53               | 0.345                                      | 1.064                         | "   |
|  | 0.00   | 0.000               | 5.85 <sup>b</sup>  | 0.562                                      | 1.051                         | "   |
|  | 25     | 48.41               | 14.11              | 0.00                                       | 0.000                         | 1.530                                     |
| 48.23  |        | 14.11               | 0.42               | 0.064                                      | 1.538                         | A+S5                                      |
| 48.17  |        | 14.08               | 0.42               | 0.064                                      | 1.536                         | "   |
| 48.21  |        | 14.10               | 0.42               | 0.064                                      | 1.541                         | "   |
| 48.22  |        | 14.11               | 0.42               | 0.064                                      | 1.534                         | "   |
| 48.21  |        | 14.10               | 0.42               | 0.064                                      | 1.537                         | "   |
| 47.73  |        | 13.87               | 0.42               | 0.063                                      | -                             | S5  |
| 47.35  |        | 13.69               | 0.42               | 0.063                                      | 1.522                         | "   |
| 46.7 <sup>b</sup>                                  |        | 13.40               | 0.45               | 0.067                                      | 1.509                         | "   |
| 43.58  |        | 12.01               | 0.55               | 0.079                                      | 1.472                         | "   |
| 39.55  |        | 10.40               | 0.86               | 0.12                                       | 1.417                         | "   |
| 38.83  |        | 10.13               | 0.95               | 0.13                                       | 1.406                         | "   |
| 36.61  |        | 9.343               | 1.31               | 0.174                                      | 1.380                         | "   |
| 35.23  |        | 8.867               | 1.51               | 0.198                                      | 1.367                         | "   |
| 34.62  |        | 8.668               | 1.66               | 0.216                                      | 1.360                         | "   |
| 34.34  |        | 8.575               | 1.71               | 0.222                                      | 1.359                         | "   |
| 32.79  |        | 8.084               | 2.13               | 0.273                                      | 1.344                         | S5+C                                      |
| 32.72  |        | 8.063               | 2.15               | 0.275                                      | 1.343                         | "   |
| 32.56  |        | 8.011               | 2.18               | 0.279                                      | 1.343                         | "   |
| 32.63  |        | 8.034               | 2.17               | 0.278                                      | 1.343                         | "   |
| 32.68  |        | 8.050               | 2.16               | 0.277                                      | 1.343                         | "   |
| 32.44  |        | 7.970               | 2.17               | 0.277                                      | 1.338                         | C   |
| 26.39  |        | 6.072               | 2.35               | 0.281                                      | 1.266                         | "   |
| 16.49  |        | 3.451               | 3.00               | 0.326                                      | 1.172                         | "   |
| 7.78   |        | 1.52                | 4.46               | 0.454                                      | 1.104                         | "   |
| 0.00   |        | 0.00                | 8.569 <sup>b</sup> | 0.8460                                     | 1.075                         | "   |
| 35   |        | 50.48               | 15.14              | 0.00                                       | 0.000                         |   |
|  | 50.04  | 15.16               | 1.01               | 0.159                                      |                               | A+S5                                      |
|  | 50.00  | 15.14               | 1.02               | 0.161                                      |                               | "   |
|  | 50.02  | 15.15               | 1.02               | 0.161                                      |                               | "   |
|  | 49.46  | 14.86               | 1.03               | 0.161                                      |                               | S5  |
|  | 47.82  | 14.05               | 1.08               | 0.165                                      |                               | "   |
|  | 46.46  | 13.42               | 1.18               | 0.177                                      |                               | "   |
|  | 44.96  | 12.75               | 1.30               | 0.192                                      |                               | "   |
|  | 42.59  | 11.76               | 1.60               | 0.230                                      |                               | "   |
|  | 40.55  | 10.96               | 1.98               | 0.278                                      |                               | "   |
|  | 38.11  | 10.08               | 2.63               | 0.362                                      |                               | "   |
|  | 38.1   | 10.08               | 2.6                | 0.358                                      |                               | S5+D(m?)                                  |

| COMPONENTS:                                      |        |                    | ORIGINAL MEASUREMENTS:                     |       |                               |   |
|--|--------|--------------------|--|-------|-------------------------------|---|
| (1) Sodium bromide; NaBr; [7647-15-6]            |        |                    | Ricci, J.E.                                |       |                               |   |
| (2) Sodium iodate; NaIO <sub>3</sub> [7681-55-2] |        |                    | J. Am. Chem. Soc. <u>1934</u> , 56, 290-5. |       |                               |   |
| (3) Water; H <sub>2</sub> O; [7732-18-5]         |        |                    |  |       |                               |   |
| EXPERIMENTAL VALUES: (Continued)                 |        |                    |  |       |                               |   |
| Composition of saturated solutions               |        |                    |  |       |                               |   |
| t/°C   | NaBr   |                    | NaIO <sub>3</sub>                          |       | Density<br>g cm <sup>-3</sup> | Nature of the<br>solid phase <sup>a</sup> |
|  | mass % | mol %              | mass %                                     | mol % |                               |   |
| 35   | 38.30  | 10.17              | 2.70                                       | 0.373 |                               | D(m?)                                     |
|  | 36.52  | 9.498              | 2.81                                       | 0.380 |                               | "   |
|  | 34.51  | 8.776              | 2.95                                       | 0.390 |                               | "   |
|  | 0.00   | 0.00               | 10.58 <sup>b</sup>                         | 1.066 |                               | C   |
| 40   | 51.5   | 15.7               | 0.00                                       | 0.00  |                               | A   |
|  | 50.84  | 15.67              | 1.37                                       | 0.220 |                               | A+S0                                      |
|  | 50.84  | 15.67              | 1.37                                       | 0.220 |                               | "   |
|  | 50.84  | 15.67              | 1.37                                       | 0.220 |                               | "   |
|  | 50.37  | 15.42              | 1.39                                       | 0.221 |                               | S0  |
|  | 50.43  | 15.46              | 1.42                                       | 0.226 |                               | "   |
|  | 49.38  | 14.94              | 1.53                                       | 0.241 |                               | "   |
|  | 48.41  | 14.49              | 1.71                                       | 0.266 |                               | "   |
|  | 47.95  | 14.27              | 1.77                                       | 0.274 |                               | S0+S5                                     |
|  | 47.96  | 14.28              | 1.80                                       | 0.279 |                               | S5  |
|  | 46.82  | 13.74              | 1.89                                       | 0.288 |                               | "   |
|  | 45.93  | 13.34              | 2.00                                       | 0.302 |                               | "   |
|  | 44.86  | 12.86              | 2.13                                       | 0.318 |                               | "   |
|  | 43.37  | 12.25              | 2.48                                       | 0.364 |                               | "   |
|  | 42.38  | 11.84              | 2.59                                       | 0.376 |                               | "   |
|  | 42.10  | 11.73              | 2.65                                       | 0.384 |                               | S5+D                                      |
|  | 41.82  | 11.62              | 2.72                                       | 0.393 |                               | "   |
|  | 41.96  | 11.67              | 2.69                                       | 0.389 |                               | "   |
|  | 42.44  | 11.85              | 2.52                                       | 0.366 |                               | D(m)                                      |
|  | 41.36  | 11.40              | 2.59                                       | 0.371 |                               | D   |
|  | 40.05  | 10.86              | 2.63                                       | 0.371 |                               | "   |
|  | 39.5   | 10.64              | 2.65                                       | 0.371 |                               | D+C                                       |
|  | 37.73  | 9.952              | 2.75                                       | 0.377 |                               | D(m)                                      |
|  | 37.29  | 9.789              | 2.80                                       | 0.382 |                               | "   |
|  | 39.06  | 10.47              | 2.68                                       | 0.373 |                               | C   |
|  | 36.79  | 9.575              | 2.62                                       | 0.355 |                               | "   |
|  | 32.08  | 7.909              | 2.77                                       | 0.355 |                               | "   |
| 27.16  | 6.355  | 3.04               | 0.370                                      |       | "                             |   |
| 20.65  | 4.539  | 3.65               | 0.417                                      |       | "                             |   |
| 0.00   | 0.000  | 11.70 <sup>b</sup> | 1.192                                      |       | "                             |   |
| 45   | 52.55  | 16.24              | 0.00                                       | 0.000 |                               | A   |
|  | 51.79  | 16.30              | 1.81                                       | 0.296 |                               | A+S0                                      |
|  | 49.91  | 15.35              | 2.08                                       | 0.333 |                               | S0  |
|  | 49.5   | 15.23              | 2.5  | 0.40  |                               | S0+D                                      |
|  | 50.29  | 15.67              | 2.56                                       | 0.415 |                               | D(m)                                      |
|  | 48.64  | 14.79              | 2.51                                       | 0.397 |                               | D   |
|  | 45.95  | 13.45              | 2.50                                       | 0.380 |                               | "   |
|  | 42.63  | 11.94              | 2.58                                       | 0.376 |                               | "   |
|  | -      | -                  | -  | -     |                               | D+C                                       |
|  | 0.00   | 0.00               | 12.83 <sup>b</sup>                         | 1.322 |                               | C   |

continued.....

| COMPONENTS:   |         |                     |                    |                     | ORIGINAL MEASUREMENTS                                     |   |
|---|---------|---------------------|--------------------|---------------------|---|---|
| (1) Sodium bromide; NaBr; [7647-15-6]   |         |                     |                    |                     | Ricci, J.E.<br>J. Am. Chem. Soc. <u>1934</u> , 56, 290-5. |   |
| (2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]  |         |                     |                    |                     |   |   |
| (3) Water; H <sub>2</sub> O; [7732-18-5]  |         |                     |                    |                     |   |   |
| EXPERIMENTAL VALUES: (Continued)  |         |                     |                    |                     |   |   |
| Composition of saturated solutions  |         |                     |                    |                     |   |   |
| t/°C  | NaBr    |                     | NaIO <sub>3</sub>  |                     | Density<br>g cm <sup>-3</sup>                             | Nature of the<br>solid phase <sup>a</sup> |
|   | mass %  | mol %<br>(compiler) | mass %             | mol %<br>(compiler) |   |   |
| 50  | 53.63   | 16.84               | 0.00               | 0.000               |   | A   |
|   | 53.0(+) | 16.92               | 1.57(-)            | 0.261               |   | A+E                                       |
|   | 52.97   | 16.90               | 1.57               | 0.260               |   | E   |
|   | 52.57   | 16.89               | 2.37               | 0.396               |   | E+S0                                      |
|   | 52.39   | 16.80               | 2.40               | 0.400               |   | S0  |
|   | 52.12   | 16.65               | 2.40               | 0.399               |   | "   |
|   | 51.40   | 16.26               | 2.49               | 0.410               |   | "   |
|   | 50.97   | 16.06               | 2.62               | 0.429               |   | S0+D                                      |
|   | 50.90   | 16.02               | 2.63               | 0.430               |   | "   |
|   | 50.91   | 16.03               | 2.64               | 0.432               |   | "   |
|   | 50.93   | 16.04               | 2.63               | 0.431               |   | "   |
|   | 50.30   | 15.69               | 2.60               | 0.422               |   | D   |
|   | 47.72   | 14.32               | 2.54               | 0.396               |   | "   |
|   | 44.74   | 12.89               | 2.56               | 0.384               |   | "   |
|   | 41.56   | 11.50               | 2.67               | 0.384               |   | "   |
|   | 38.56   | 10.29               | 2.86               | 0.397               |   | "   |
|   | 32.41   | 8.087               | 3.41               | 0.442               |   | "   |
|   | 26.02   | 6.105               | 4.30               | 0.525               |   | "   |
|   | 23.54   | 5.403               | 4.73               | 0.564               |   | "   |
|   | 21.46   | 4.841               | 5.15               | 0.604               |   | D+C                                       |
|   | 19.75   | 4.365               | 4.93               | 0.566               |   | C   |
|   | 19.57   | 4.313               | 4.86               | 0.557               |   | "   |
|   | 13.28   | 2.790               | 6.28               | 0.686               |   | "   |
|   | 6.63    | 1.34                | 9.03               | 0.952               |   | "   |
|   | 0.00    | 0.00                | 13.49 <sup>b</sup> | 1.400               |   | "   |
| <sup>a</sup> A = NaBr.2H <sub>2</sub> O; B = NaIO <sub>3</sub> .5H <sub>2</sub> O; C = NaIO <sub>3</sub> .H <sub>2</sub> O; D = NaIO <sub>3</sub> ; E = NaBr;<br>S5 = 2NaIO <sub>3</sub> .3NaBr.15H <sub>2</sub> O; S0 = 2NaIO <sub>3</sub> .3NaBr.10H <sub>2</sub> O; m = metastable |         |                     |                    |                     |   |   |
| <sup>b</sup> For the binary system the compiler computes the following:   |         |                     |                    |                     |   |   |
| soly of NaIO <sub>3</sub> = 0.2929 mol kg <sup>-1</sup> at 5°C  |         |                     |                    |                     |   |   |
| = 0.3163 mol kg <sup>-1</sup> at 15°C   |         |                     |                    |                     |   |   |
| = 0.4736 mol kg <sup>-1</sup> at 25°C   |         |                     |                    |                     |   |   |
| = 0.5979 mol kg <sup>-1</sup> at 35°C   |         |                     |                    |                     |   |   |
| = 0.6696 mol kg <sup>-1</sup> at 40°C   |         |                     |                    |                     |   |   |
| = 0.7438 mol kg <sup>-1</sup> at 45°C   |         |                     |                    |                     |   |   |
| = 0.7880 mol kg <sup>-1</sup> at 50°C   |         |                     |                    |                     |   |   |
| COMMENTS AND/OR ADDITIONAL DATA:  |         |                     |                    |                     |   |   |
| Isotherms based on mass % units are reproduced below.   |         |                     |                    |                     |   |   |
| continued.....  |         |                     |                    |                     |   |   |

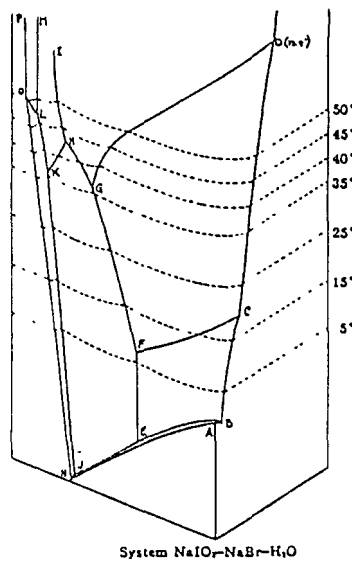
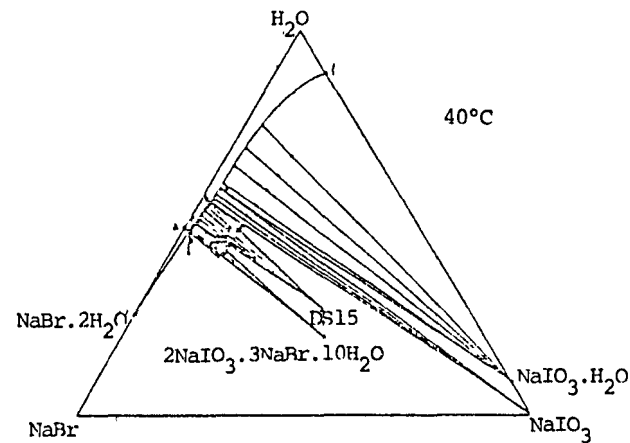
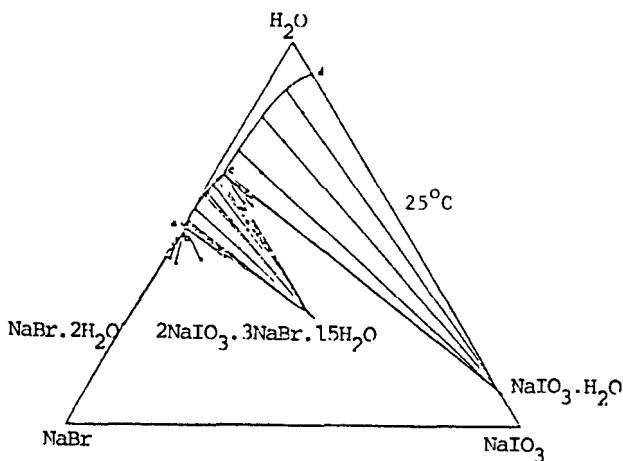
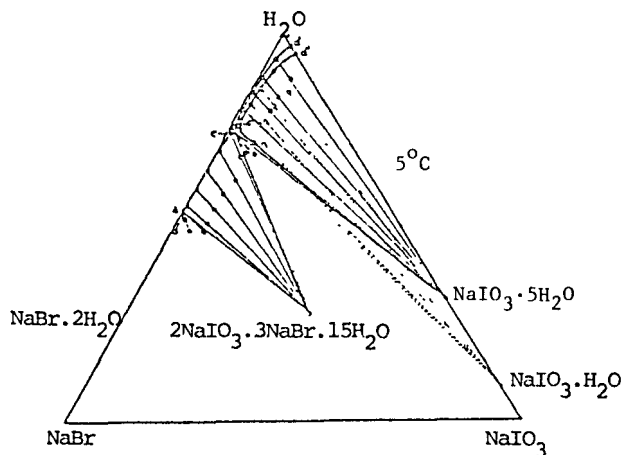
COMPONENTS:

- (1) Sodium bromide; NaBr; [7647-15-6]
- (2) Sodium iodate; NaIO<sub>3</sub>; [7681-55-2]
- (3) Water; H<sub>2</sub>O; [7732-18-5]

ORIGINAL MEASUREMENTS:

Ricci, J.E.  
*J. Am. Chem. Soc.* 1934, 56, 290-5.

COMMENTS AND/OR ADDITIONAL DATA: (Continued)



|  |        |                            |                   |   |                               |   |
|--|--------|----------------------------|-------------------|---|-------------------------------|---|
| <b>COMPONENTS:</b>   |        |                            |                   | <b>ORIGINAL MEASUREMENTS:</b>   |                               |   |
| (1) Sodium iodide; NaI; [7681-82-5]  |        |                            |                   | Hill, A.E.; Willson, H.S.; Bishop, J.A.   |                               |   |
| (2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]   |        |                            |                   | J. Am. Chem. Soc. <u>1933</u> , 55, 520-6.  |                               |   |
| (3) Water; H <sub>2</sub> O; [7732-18-5]   |        |                            |                   |   |                               |   |
| <b>VARIABLES:</b>  |        |                            |                   | <b>PREPARED BY:</b>   |                               |   |
| Composition  |        |                            |                   | Hiroshi Miyamoto  |                               |   |
| T/K = 281 - 313  |        |                            |                   |   |                               |   |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions   |        |                            |                   |   |                               |   |
| t/°C   | mass % | NaI<br>mol %<br>(compiler) | mass %            | NaIO <sub>3</sub><br>mol %<br>(compiler)  | Density<br>g cm <sup>-3</sup> | Nature of the<br>solid phase <sup>a</sup> |
| 8  | 0.00   | 0.00                       | 3.89 <sup>b</sup> | 0.367   | 1.035                         | A   |
|  | 6.05   | 0.783                      | 1.99              | 0.195   | 1.069                         | "   |
|  | 17.18  | 2.471                      | 1.44              | 0.157   | 1.169                         | "   |
|  | 19.47  | 2.882                      | 1.84              | 0.206   | 1.196                         | A+S                                       |
|  | 25.20  | 3.924                      | 0.72              | 0.085   | 1.249                         | S   |
|  | 40.70  | 7.629                      | 0.08              | 0.011   | 1.445                         | "   |
|  | 57.87  | 14.17                      | 0.02              | 0.004   | -                             | "   |
|  | 62.44  | 16.66                      | 0.02              | 0.004   | 1.861                         | S+D                                       |
|  | 62.49  | 16.68                      | 0.00              | 0.000   | -                             | D   |
|  | 25     | 0.00                       | 0.00              | 8.67 <sup>b</sup>   | 0.857                         | 1.077                                     |
| 11.57  |        | 1.617                      | 4.23              | 0.448   | 1.107                         | "   |
| 24.54  |        | 3.882                      | 2.68              | 0.321   | 1.253                         | "   |
| 28.70  |        | 4.758                      | 2.48              | 0.311   | 1.290                         | "   |
| 31.72  |        | 5.454                      | 2.41              | 0.314   | 1.340                         | "   |
| 31.74  |        | 5.455                      | 2.36              | 0.307   | 1.340                         | "   |
| 31.99  |        | 5.515                      | 2.36              | 0.308   | 1.341                         | B+S                                       |
| 33.04  |        | 5.749                      | 2.04              | 0.269   | 1.352                         | S   |
| 36.64  |        | 6.607                      | 1.22              | 0.167   | 1.377                         | "   |
| 46.08  |        | 9.359                      | 0.31              | 0.048   | -                             | "   |
| 56.83  |        | 13.70                      | 0.17              | 0.031   | 1.722                         | "   |
| continued.....   |        |                            |                   |   |                               |   |
| <b>AUXILIARY INFORMATION</b>   |        |                            |                   |   |                               |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b>   |        |                            |                   | <b>SOURCE AND PURITY OF MATERIALS:</b>  |                               |   |
| The salts were weighed into stoppered Pyrex tubes with weighed amounts of water and stirred by mechanical inversion in a thermostat for 4-7 days.<br>Small samples of the saturated solution were withdrawn by suction through a filter into a pipet. One sample was dried to constant weight in the oven, while a second was analyzed for iodate.<br>Iodate was determined by iodometry, thio-sulfate solution being used in the titration. The water was determined gravimetrically (after evaporation). |        |                            |                   | Sodium iodate was recrystallized from water and dehydrated in an electric oven at 100°C. Sodium iodide (c.p. grade) was purified by recrystallization and dried in an electric oven at 100°C. |                               |   |
|  |        |                            |                   | <b>ESTIMATED ERROR:</b>   |                               |   |
|  |        |                            |                   | Soly: precision of the analyses about 0.3 %.<br>Temp: not given.  |                               |   |
|  |        |                            |                   | <b>REFERENCES:</b>  |                               |   |
|  |        |                            |                   |   |                               |   |

|   |   |
|---|---|
| <b>COMPONENTS:</b><br>(1) Sodium iodide; NaI; [7681-82-5]<br>(2) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]<br>(3) Water; H <sub>2</sub> O; [7732-18-5] | <b>ORIGINAL MEASUREMENTS:</b><br>Hill, A.E.; Willson, H.S.; Bishop, J.A.<br><i>J. Am. Chem. Soc.</i> <u>1933</u> , 55, 520-6. |
|---|---|

**EXPERIMENTAL VALUES: (Continued)**

## Composition of saturated solutions

| t/°C  | NaI    |                     | NaIO <sub>3</sub>  |                     | Density<br>g cm <sup>-3</sup> | Nature of the<br>solid phase <sup>a</sup> |
|-------|--------|---------------------|--------------------|---------------------|-------------------------------|---|
|       | mass % | mol %<br>(compiler) | mass %             | mol %<br>(compiler) |                               |   |
| 25    | 64.67  | 18.06               | 0.08               | 0.017               | -                             | S+D                                       |
|       | 64.72  | 18.06               | 0.00               | 0.000               | -                             | D   |
| 40    | 0.00   | 0.000               | 11.70 <sup>b</sup> | 1.192               |                               | B   |
|       | 15.33  | 2.254               | 5.24               | 0.584               |                               | "   |
|       | 18.16  | 2.738               | 4.74               | 0.541               |                               | "   |
|       | 19.64  | 3.001               | 4.47               | 0.517               |                               | "   |
|       | 22.06  | 3.441               | 3.90               | 0.461               |                               | "   |
|       | 26.85  | 4.408               | 3.49               | 0.434               |                               | C   |
|       | 33.65  | 5.970               | 2.92               | 0.392               |                               | "   |
|       | 40.52  | 7.877               | 2.78               | 0.409               |                               | "   |
|       | 41.16  | 8.076               | 2.79               | 0.415               |                               | C+S                                       |
|       | 41.30  | 8.121               | 2.80               | 0.417               |                               | S   |
|       | 42.55  | 8.510               | 2.72               | 0.412               |                               | "   |
|       | 51.97  | 11.62               | 0.58               | 0.098               |                               | "   |
|       | 64.40  | 18.04               | 0.47               | 0.100               |                               | "   |
|       | 66.15  | 19.15               | 0.32               | 0.070               |                               | "   |
| 67.58 | 20.16  | 0.28                | 0.063              |                     | S+D                           |   |
| 67.35 | 19.87  | 0.00                | 0.000              |                     | D                             |   |

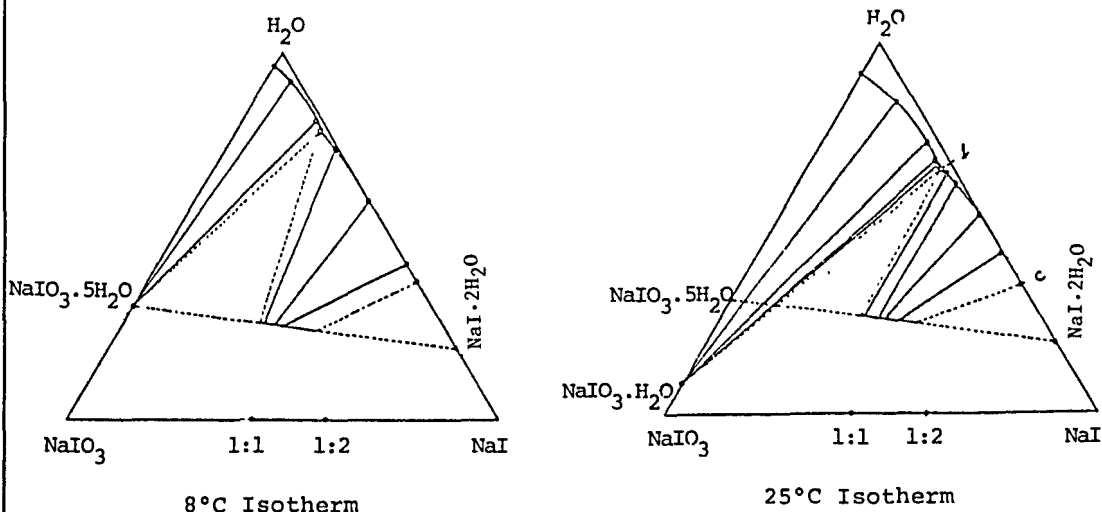
<sup>a</sup> A = NaIO<sub>3</sub>·5H<sub>2</sub>O; B = NaIO<sub>3</sub>·H<sub>2</sub>O; C = NaIO<sub>3</sub>; D = NaI·2H<sub>2</sub>O; S = solid solution

<sup>b</sup> For the binary system the compiler computes the following:

solv of NaIO<sub>3</sub> = 0.205 mol kg<sup>-1</sup> at 8°C  
 = 0.480 mol kg<sup>-1</sup> at 25°C  
 = 0.6696 mol kg<sup>-1</sup> at 40°C

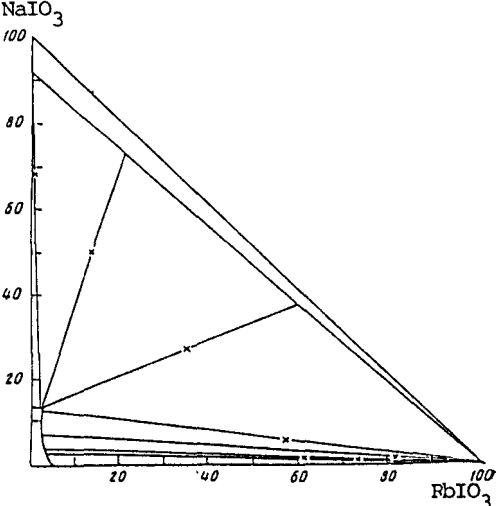
**COMMENTS AND/OR ADDITIONAL DATA:**

The solubility isotherms are reproduced below (based on mass % units).



| <b>COMPONENTS:</b>  |                    | <b>ORIGINAL MEASUREMENTS:</b>                |  |                     |                               |   |
|---|--------------------|--|--|---------------------|-------------------------------|---|
| (1) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]  |                    | Hill, A.E.; Ricci, J.E.                      |  |                     |                               |   |
| (2) Potassium iodate; KIO <sub>3</sub> ; [7758-05-6]  |                    | J. Am. Chem. Soc. <u>1931</u> , 53, 4305-15. |  |                     |                               |   |
| (3) Water; H <sub>2</sub> O; [7732-18-5]  |                    |  |  |                     |                               |   |
| <b>VARIABLES:</b>   |                    | <b>PREPARED BY:</b>                          |  |                     |                               |   |
| Composition at 278.2, 298.2, 323.2 K  |                    | Hiroshi Miyamoto                             |  |                     |                               |   |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions  |                    |  |  |                     |                               |   |
| t/°C  | NaIO <sub>3</sub>  |  | KIO <sub>3</sub>                           |                     | Density<br>g cm <sup>-3</sup> | Nature of the<br>solid phase <sup>a</sup> |
|   | mass %             | mol %<br>(compiler)                          | mass %                                     | mol %<br>(compiler) |                               |   |
| 5   | 0.00               | 0.000  | 5.16                                       | 0.456               | 1.043                         | A   |
|   | 1.41               | 0.136  | 4.71                                       | 0.420               | 1.051                         | "   |
|   | 2.17               | 0.211  | 4.72                                       | 0.424               | 1.060                         | A+B                                       |
|   | 2.48               | 0.238  | 3.19                                       | 0.283               | 1.046                         | B   |
|   | 3.28 <sup>b</sup>  | 0.308  | 0.00                                       | 0.000               | 1.028                         | "   |
| 25  | 0.00               | 0.000  | 8.45                                       | 0.771               | 1.071                         | A   |
|   | 4.26               | 0.433  | 7.09                                       | 0.666               | 1.098                         | "   |
|   | 7.13               | 0.743  | 6.73                                       | 0.649               | 1.126                         | A+C                                       |
|   | 7.79               | 0.793  | 3.79                                       | 0.357               | 1.103                         | C   |
|   | 8.57 <sup>b</sup>  | 0.846  | 0.00                                       | 0.000               | 1.074                         | "   |
| 50  | 0.00               | 0.000  | 13.21                                      | 1.265               | -                             | A   |
|   | 3.92               | 0.417  | 11.92                                      | 1.173               | -                             | "   |
|   | 7.70               | 0.847  | 11.14                                      | 1.133               | -                             | "   |
|   | 10.92              | 1.237  | 10.61                                      | 1.112               | -                             | A+C                                       |
|   | 11.41              | 1.261  | 7.93                                       | 0.810               | -                             | C   |
|   | 12.55              | 1.349  | 4.24                                       | 0.421               | -                             | "   |
|   | 13.49 <sup>b</sup> | 1.400  | 0.00                                       | 0.000               | -                             | "   |
| <sup>a</sup> A = KIO <sub>3</sub> ;      B = NaIO <sub>3</sub> ·5H <sub>2</sub> O;      C = NaIO <sub>3</sub> ·H <sub>2</sub> O<br><sup>b</sup> For the binary system the compiler computes the following:<br>soly of NaIO <sub>3</sub> = 0.171 mol kg <sup>-1</sup> at 5°C; = 0.474 mol kg <sup>-1</sup> at 25°C;<br>= 0.7880 mol kg <sup>-1</sup> at 50°C.  |                    |  |  |                     |                               |   |
| <b>AUXILIARY INFORMATION</b>  |                    |  |  |                     |                               |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b>  |                    |  | <b>COMMENTS AND/OR ADDITIONAL DATA:</b>    |                     |                               |   |
| The complexes used for the ternary system were made up from weighed amounts of water, dried NaIO <sub>3</sub> and KIO <sub>3</sub> . For the 5°C isotherm, the solids were first dissolved by heating, and the solutions were seeded after cooling. The solutions were agitated in a thermostat at the desired temperature for about thirteen days.<br>For the analysis, samples of filtered solution were evaporated to dryness at 110°C, and other samples were titrated for iodate by iodometry. |                    |  |  |                     |                               |   |
| <b>SOURCE AND PURITY OF MATERIALS:</b>  |                    |  |  |                     |                               |   |
| Nothing specified.  |                    |  |  |                     |                               |   |
| <b>ESTIMATED ERROR:</b>   |                    |  | 5°C, 25°C, 50°C Isotherm<br>(mass % units) |                     |                               |   |
| Nothing specified, but the compiler assumes that the agreement between duplicate analyses was around ± 0.5 %.   |                    |  |  |                     |                               |   |



| <b>COMPONENTS:</b><br>(1) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]<br>(2) Rubidium iodate; RbIO <sub>3</sub> ; [13446-76-9]<br>(3) Water; H <sub>2</sub> O; [7732-18-5]   | <b>ORIGINAL MEASUREMENTS:</b><br>Vinogradov, E.E.; Karataeva, I.M.<br><br><i>Zh. Neorg. Khim.</i> 1982, 27, 2155-7;<br><i>Russ. J. Inorg. Chem. (Engl. Transl.)</i><br>1982, 27, 1218-9.   |                     |                                    |                     |  |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|---|--|---------------------|------------------------------------|---------------------|--|--|--|-------------------|--|-------------------|--|--|--------|---------------------|--------|---------------------|--|----|--------------------|-------|---|---|---|-------|-------|------|-------|---|-------|-------|------|-------|-----|-------|-------|------|-------|---|-------|-------|------|-------|---|------|-------|------|-------|---|------|-------|------|-------|---|------|-------|------|-------|---|---|---|-------------------|-------|---|
| <b>VARIABLES:</b><br><br>Composition at 323.2 K   | <b>PREPARED BY:</b><br><br>Hiroshi Miyamoto  |                     |                                    |                     |  |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
| <b>EXPERIMENTAL VALUES:</b> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th rowspan="2">t/°C</th> <th colspan="4">Composition of saturated solutions</th> <th rowspan="2">Nature of the solid phase<sup>a</sup></th> </tr> <tr> <th colspan="2">NaIO<sub>3</sub></th> <th colspan="2">RbIO<sub>3</sub></th> </tr> <tr> <th></th> <th>mass %</th> <th>mol %<br/>(compiler)</th> <th>mass %</th> <th>mol %<br/>(compiler)</th> <th></th> </tr> </thead> <tbody> <tr> <td rowspan="10">50</td> <td>13.52<sup>b</sup></td> <td>1.403</td> <td>-</td> <td>-</td> <td>A</td> </tr> <tr> <td>13.40</td> <td>1.419</td> <td>1.96</td> <td>0.158</td> <td>"</td> </tr> <tr> <td>13.77</td> <td>1.465</td> <td>2.03</td> <td>0.164</td> <td>A+B</td> </tr> <tr> <td>13.74</td> <td>1.461</td> <td>2.05</td> <td>0.166</td> <td>"</td> </tr> <tr> <td>12.20</td> <td>1.283</td> <td>2.50</td> <td>0.200</td> <td>B</td> </tr> <tr> <td>7.25</td> <td>0.723</td> <td>2.30</td> <td>0.174</td> <td>"</td> </tr> <tr> <td>3.96</td> <td>0.383</td> <td>2.32</td> <td>0.170</td> <td>"</td> </tr> <tr> <td>2.92</td> <td>0.282</td> <td>3.29</td> <td>0.241</td> <td>"</td> </tr> <tr> <td>-</td> <td>-</td> <td>4.39<sup>b</sup></td> <td>0.317</td> <td>"</td> </tr> </tbody> </table> <p><sup>a</sup> A = NaIO<sub>3</sub>·H<sub>2</sub>O;    B = RbIO<sub>3</sub></p> <p><sup>b</sup> For the binary systems the compiler computes the following:</p> <p style="padding-left: 40px;">soly of NaIO<sub>3</sub> = 0.7900 mol kg<sup>-1</sup></p> <p style="padding-left: 40px;">soly of RbIO<sub>3</sub> = 0.176 mol kg<sup>-1</sup></p> |  | t/°C                | Composition of saturated solutions |                     |  |  | Nature of the solid phase <sup>a</sup> | NaIO <sub>3</sub> |  | RbIO <sub>3</sub> |  |  | mass % | mol %<br>(compiler) | mass % | mol %<br>(compiler) |  | 50 | 13.52 <sup>b</sup> | 1.403 | - | - | A | 13.40 | 1.419 | 1.96 | 0.158 | " | 13.77 | 1.465 | 2.03 | 0.164 | A+B | 13.74 | 1.461 | 2.05 | 0.166 | " | 12.20 | 1.283 | 2.50 | 0.200 | B | 7.25 | 0.723 | 2.30 | 0.174 | " | 3.96 | 0.383 | 2.32 | 0.170 | " | 2.92 | 0.282 | 3.29 | 0.241 | " | - | - | 4.39 <sup>b</sup> | 0.317 | " |
| t/°C  | Composition of saturated solutions   |                     |                                    |                     | Nature of the solid phase <sup>a</sup> |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | NaIO <sub>3</sub>  |                     | RbIO <sub>3</sub>                  |                     |  |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | mass %   | mol %<br>(compiler) | mass %                             | mol %<br>(compiler) |  |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
| 50  | 13.52 <sup>b</sup>   | 1.403               | -                                  | -                   | A                                      |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | 13.40  | 1.419               | 1.96                               | 0.158               | "                                      |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | 13.77  | 1.465               | 2.03                               | 0.164               | A+B                                    |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | 13.74  | 1.461               | 2.05                               | 0.166               | "                                      |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | 12.20  | 1.283               | 2.50                               | 0.200               | B                                      |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | 7.25   | 0.723               | 2.30                               | 0.174               | "                                      |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | 3.96   | 0.383               | 2.32                               | 0.170               | "                                      |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | 2.92   | 0.282               | 3.29                               | 0.241               | "                                      |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | -  | -                   | 4.39 <sup>b</sup>                  | 0.317               | "                                      |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
|   | <b>AUXILIARY INFORMATION</b>   |                     |                                    |                     |  |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Probably the isothermal method was used. Equilibrium was established after 4-5 days. Rubidium and iodate ions in the liquid and solid phases were analyzed. The sodium content was determined by difference. The composition of the solid phase was determined by X-ray analysis.   | <b>COMMENTS AND/OR ADDITIONAL DATA:</b><br>The phase diagram is given below (based on mass % units). <div style="text-align: center;">  </div> |                     |                                    |                     |  |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
| <b>SOURCE AND PURITY OF MATERIALS:</b><br>No information given.   |  |                     |                                    |                     |  |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |
| <b>ESTIMATED ERROR:</b><br>Nothing specified.   |  |                     |                                    |                     |  |  |  |                   |  |                   |  |  |        |                     |        |                     |  |    |                    |       |   |   |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |      |       |      |       |   |      |       |      |       |   |      |       |      |       |   |   |   |                   |       |   |

|   |   |  |   |                     |  |  |
|---|---|--|---|---------------------|--|--|
| <b>COMPONENTS:</b>  |   | <b>ORIGINAL MEASUREMENTS:</b>  |   |                     |  |  |
| (1) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]  |   | Vinogradov, E.E.; Karataeva, I.M.  |   |                     |  |  |
| (2) Cesium iodate; CsIO <sub>3</sub> ; [13454-81-4]   |   | Zh. Neorg. Khim. 1982, 27, 2155-7;<br>Russ. J. Inorg. Chem. (Engl. Transl.)<br>1982, 27, 1218-9. |   |                     |  |  |
| (3) Water; H <sub>2</sub> O; [7732-18-5]  |   |  |   |                     |  |  |
| <b>VARIABLES:</b>   |   | <b>PREPARED BY:</b>  |   |                     |  |  |
| Composition at 323.2 K  |   | Hiroschi Miyamoto  |   |                     |  |  |
| <b>EXPERIMENTAL VALUES:</b>   |   |  |   |                     |  |  |
| Composition of saturated solutions  |   |  |   |                     |  |  |
| t/°C  | NaIO <sub>3</sub>   |  | CsIO <sub>3</sub>   |                     | Nature of the solid phase <sup>b</sup> |  |
|   | mass %  | mol %<br>(compiler)  | mass %  | mol %<br>(compiler) |  |  |
| 50  | 13.52 <sup>b</sup>  | 1.403  | -   | -                   | A                                      |  |
|   | 12.15   | 1.262  | 1.41  | 0.0942              | "                                      |  |
|   | 12.46   | 1.309  | 2.16  | 0.146               | A+B                                    |  |
|   | 12.46   | 1.306  | 1.96  | 0.132               | "                                      |  |
|   | 12.49   | 1.314  | 2.23  | 0.151               | "                                      |  |
|   | 12.61   | 1.325  | 2.02  | 0.136               | "                                      |  |
|   | 11.77   | 1.231  | 2.40  | 0.161               | B                                      |  |
|   | 10.27   | 1.054  | 2.12  | 0.140               | "                                      |  |
|   | 6.93  | 0.688  | 2.18  | 0.139               | "                                      |  |
|   | 3.34  | 0.324  | 3.44  | 0.215               | "                                      |  |
|   | -   | -  | 5.07 <sup>b</sup>   | 0.312               | "                                      |  |
|   | <sup>a</sup> A = NaIO <sub>3</sub> ·H <sub>2</sub> O;      B = CsIO <sub>3</sub>  |  |   |                     |  |  |
|   | <sup>b</sup> For binary systems the compiler computes the following:<br>soly of NaIO <sub>3</sub> = 0.7900 mol kg <sup>-1</sup><br>soly of CsIO <sub>3</sub> = 0.174 mol kg <sup>-1</sup> |  |   |                     |  |  |
| <b>AUXILIARY INFORMATION</b>  |   |  |   |                     |  |  |
| <b>METHOD/APPARATUS/PROCEDURE:</b>  |   |  | <b>COMMENTS AND/OR ADDITIONAL DATA:</b>                   |                     |  |  |
| Probably the isothermal method was used. Equilibrium was established after 4-5 days. Cesium and iodate ions in the liquid and solid phases were analyzed. The sodium content was determined by difference. The composition of the solid phase was determined by X-ray analysis. |   |  | The phase diagram is given below (based on mass % units). |                     |  |  |
| <b>SOURCE AND PURITY OF MATERIALS:</b>  |   |  |   |                     |  |  |
| No information given.   |   |  |   |                     |  |  |
| <b>ESTIMATED ERROR:</b>   |   |  |   |                     |  |  |
| Nothing specified.  |   |  |   |                     |  |  |

| <b>COMPONENTS:</b><br>(1) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]<br>(2) Aluminum iodate; Al(IO <sub>3</sub> ) <sub>3</sub> ; [15123-75-3]<br>(3) Water; H <sub>2</sub> O; [7732-18-5]   | <b>ORIGINAL MEASUREMENTS:</b><br>Shklovskaya, R.M.; Arkhipov, S.M.; Kidyarov, B.I.; Tokareva, A.G.<br><i>Zh. Neorg. Khim.</i> 1980, 25, 1423-4;<br><i>Russ. J. Inorg. Chem. (Engl. Transl.)</i> 1980, 25, 791.                |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
|---|---|-----------------------------------|---------------------|--|--|--|--------|---------------------|--------|---------------------|-------------------|-------|---|---|---|------|-------|------|-------|---|------|-------|------|--------|-----|------|-------|------|--------|---|------|-------|------|--------|---|------|-------|------|--------|---|------|-------|------|--------|---|------|-------|------|-------|---|------|-------|------|-------|---|-----|------|------|-------|---|---|---|-------------------|-------|---|
| <b>VARIABLES:</b><br>Composition at 298.2 K   | <b>PREPARED BY:</b><br>Hiroshi Miyamoto   |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions at 25°C  |   |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| <table border="1"> <thead> <tr> <th colspan="2">NaIO<sub>3</sub></th> <th colspan="2">Al(IO<sub>3</sub>)<sub>3</sub></th> <th rowspan="2">Nature of the solid phase<sup>a</sup></th> </tr> <tr> <th>mass %</th> <th>mol %<br/>(compiler)</th> <th>mass %</th> <th>mol %<br/>(compiler)</th> </tr> </thead> <tbody> <tr> <td>8.66<sup>b</sup></td> <td>0.856</td> <td>-</td> <td>-</td> <td>A</td> </tr> <tr> <td>8.30</td> <td>0.821</td> <td>0.38</td> <td>0.013</td> <td>"</td> </tr> <tr> <td>8.15</td> <td>0.819</td> <td>2.02</td> <td>0.0728</td> <td>A+B</td> </tr> <tr> <td>6.83</td> <td>0.678</td> <td>2.21</td> <td>0.0787</td> <td>B</td> </tr> <tr> <td>6.44</td> <td>0.638</td> <td>2.38</td> <td>0.0846</td> <td>"</td> </tr> <tr> <td>6.30</td> <td>0.624</td> <td>2.45</td> <td>0.0871</td> <td>"</td> </tr> <tr> <td>5.14</td> <td>0.504</td> <td>2.66</td> <td>0.0936</td> <td>"</td> </tr> <tr> <td>3.60</td> <td>0.350</td> <td>3.18</td> <td>0.111</td> <td>"</td> </tr> <tr> <td>1.52</td> <td>0.146</td> <td>4.15</td> <td>0.143</td> <td>"</td> </tr> <tr> <td>0.9</td> <td>0.09</td> <td>4.48</td> <td>0.154</td> <td>"</td> </tr> <tr> <td>-</td> <td>-</td> <td>5.70<sup>b</sup></td> <td>0.197</td> <td>"</td> </tr> </tbody> </table> |   | NaIO <sub>3</sub>                 |                     | Al(IO <sub>3</sub> ) <sub>3</sub>      |  | Nature of the solid phase <sup>a</sup> | mass % | mol %<br>(compiler) | mass % | mol %<br>(compiler) | 8.66 <sup>b</sup> | 0.856 | - | - | A | 8.30 | 0.821 | 0.38 | 0.013 | " | 8.15 | 0.819 | 2.02 | 0.0728 | A+B | 6.83 | 0.678 | 2.21 | 0.0787 | B | 6.44 | 0.638 | 2.38 | 0.0846 | " | 6.30 | 0.624 | 2.45 | 0.0871 | " | 5.14 | 0.504 | 2.66 | 0.0936 | " | 3.60 | 0.350 | 3.18 | 0.111 | " | 1.52 | 0.146 | 4.15 | 0.143 | " | 0.9 | 0.09 | 4.48 | 0.154 | " | - | - | 5.70 <sup>b</sup> | 0.197 | " |
| NaIO <sub>3</sub>   |   | Al(IO <sub>3</sub> ) <sub>3</sub> |                     | Nature of the solid phase <sup>a</sup> |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| mass %  | mol %<br>(compiler)   | mass %                            | mol %<br>(compiler) |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 8.66 <sup>b</sup>   | 0.856   | -                                 | -                   | A                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 8.30  | 0.821   | 0.38                              | 0.013               | "                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 8.15  | 0.819   | 2.02                              | 0.0728              | A+B                                    |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 6.83  | 0.678   | 2.21                              | 0.0787              | B                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 6.44  | 0.638   | 2.38                              | 0.0846              | "                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 6.30  | 0.624   | 2.45                              | 0.0871              | "                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 5.14  | 0.504   | 2.66                              | 0.0936              | "                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 3.60  | 0.350   | 3.18                              | 0.111               | "                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 1.52  | 0.146   | 4.15                              | 0.143               | "                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| 0.9   | 0.09  | 4.48                              | 0.154               | "                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| -   | -   | 5.70 <sup>b</sup>                 | 0.197               | "                                      |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| <sup>a</sup> A = NaIO <sub>3</sub> ·H <sub>2</sub> O      B = Al(IO <sub>3</sub> ) <sub>3</sub> ·6H <sub>2</sub> O  |   |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| <sup>b</sup> For binary systems the compiler computes the following:<br>soly of NaIO <sub>3</sub> = 0.479 mol kg <sup>-1</sup><br>soly of Al(IO <sub>3</sub> ) <sub>3</sub> = 0.110 mol kg <sup>-1</sup>  |   |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| <b>AUXILIARY INFORMATION</b>  |   |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>The isothermal method was used. Equilibrium was reached within 15-20 days. The aluminum content in the co-existing phases was determined by complexometric titration. Sodium was determined by the flame photometry. The photometry was carried out on solutions in which the sodium concentration did not exceed 10 μg dm <sup>-3</sup> .  | <b>SOURCE AND PURITY OF MATERIALS:</b><br>Aluminum iodate hexahydrate was synthesized from iodic acid and aluminum hydroxide. Chemically pure grade sodium iodate monohydrate was recrystallized twice from aqueous solution. |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
|   | <b>ESTIMATED ERROR:</b><br>Soly: 1-3 rel %.<br>Temp: precision ± 0.1 K.   |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |
|   | <b>REFERENCES:</b>  |                                   |                     |  |  |  |        |                     |        |                     |                   |       |   |   |   |      |       |      |       |   |      |       |      |        |     |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |        |   |      |       |      |       |   |      |       |      |       |   |     |      |      |       |   |   |   |                   |       |   |

| <b>COMPONENTS:</b><br>(1) Sodium iodate; NaIO <sub>3</sub> ; [7681-55-2]<br>(2) Hafnium iodate; Hf(IO <sub>3</sub> ) <sub>4</sub> ; [19630-06-9]<br>(3) Water; H <sub>2</sub> O; [7732-18-5]   | <b>ORIGINAL MEASUREMENTS:</b><br>Shklovskaya, R.M.; Arkhipov, S.M.;<br>Kidyarov, B.I.; Poleva, G.V.; Timofeev, S.I.<br><i>Zh. Neorg. Khim.</i> 1983, 28, 2435-6;<br><i>Russ. J. Inorg. Chem. (Engl. Transl.)</i><br>1983, 28, 1384-5. |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
|--|---|-----------------------------------|------------------------|--|--|--|--------|---------------------|--------|---------------------|---|---|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|---|------|-------|---------|------------------------|-----|-------------------|-------|---|---|---|
| <b>VARIABLES:</b><br>Composition at 298.2 K  | <b>PREPARED BY:</b><br>Hiroshi Miyamoto   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions at 25°C   |   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| <table border="1"> <thead> <tr> <th colspan="2">NaIO<sub>3</sub></th> <th colspan="2">Hf(IO<sub>3</sub>)<sub>4</sub></th> <th rowspan="2">Nature of the solid phase<sup>a</sup></th> </tr> <tr> <th>mass %</th> <th>mol %<br/>(compiler)</th> <th>mass %</th> <th>mol %<br/>(compiler)</th> </tr> </thead> <tbody> <tr> <td>-</td> <td>-</td> <td>0.00037</td> <td>7.6 x 10<sup>-6</sup></td> <td>A</td> </tr> <tr> <td>0.87</td> <td>0.080</td> <td>0.00036</td> <td>7.4 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>1.45</td> <td>0.134</td> <td>0.00034</td> <td>7.1 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>2.38</td> <td>0.221</td> <td>0.00027</td> <td>5.7 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>3.29</td> <td>0.309</td> <td>0.00025</td> <td>5.3 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>4.03</td> <td>0.381</td> <td>0.00023</td> <td>4.9 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>4.89</td> <td>0.466</td> <td>0.00020</td> <td>4.3 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>5.68</td> <td>0.545</td> <td>0.00018</td> <td>3.9 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>6.38</td> <td>0.617</td> <td>0.00020</td> <td>4.4 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>7.18</td> <td>0.699</td> <td>0.00032</td> <td>7.0 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>8.23</td> <td>0.810</td> <td>0.00034</td> <td>7.5 x 10<sup>-6</sup></td> <td>"</td> </tr> <tr> <td>8.62</td> <td>0.851</td> <td>0.00035</td> <td>7.8 x 10<sup>-6</sup></td> <td>A+B</td> </tr> <tr> <td>8.66<sup>b</sup></td> <td>0.856</td> <td>-</td> <td>-</td> <td>B</td> </tr> </tbody> </table> |   | NaIO <sub>3</sub>                 |                        | Hf(IO <sub>3</sub> ) <sub>4</sub>      |  | Nature of the solid phase <sup>a</sup> | mass % | mol %<br>(compiler) | mass % | mol %<br>(compiler) | - | - | 0.00037 | 7.6 x 10 <sup>-6</sup> | A | 0.87 | 0.080 | 0.00036 | 7.4 x 10 <sup>-6</sup> | " | 1.45 | 0.134 | 0.00034 | 7.1 x 10 <sup>-6</sup> | " | 2.38 | 0.221 | 0.00027 | 5.7 x 10 <sup>-6</sup> | " | 3.29 | 0.309 | 0.00025 | 5.3 x 10 <sup>-6</sup> | " | 4.03 | 0.381 | 0.00023 | 4.9 x 10 <sup>-6</sup> | " | 4.89 | 0.466 | 0.00020 | 4.3 x 10 <sup>-6</sup> | " | 5.68 | 0.545 | 0.00018 | 3.9 x 10 <sup>-6</sup> | " | 6.38 | 0.617 | 0.00020 | 4.4 x 10 <sup>-6</sup> | " | 7.18 | 0.699 | 0.00032 | 7.0 x 10 <sup>-6</sup> | " | 8.23 | 0.810 | 0.00034 | 7.5 x 10 <sup>-6</sup> | " | 8.62 | 0.851 | 0.00035 | 7.8 x 10 <sup>-6</sup> | A+B | 8.66 <sup>b</sup> | 0.856 | - | - | B |
| NaIO <sub>3</sub>  |   | Hf(IO <sub>3</sub> ) <sub>4</sub> |                        | Nature of the solid phase <sup>a</sup> |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| mass %   | mol %<br>(compiler)   | mass %                            | mol %<br>(compiler)    |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| -  | -   | 0.00037                           | 7.6 x 10 <sup>-6</sup> | A                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 0.87   | 0.080   | 0.00036                           | 7.4 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 1.45   | 0.134   | 0.00034                           | 7.1 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 2.38   | 0.221   | 0.00027                           | 5.7 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 3.29   | 0.309   | 0.00025                           | 5.3 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 4.03   | 0.381   | 0.00023                           | 4.9 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 4.89   | 0.466   | 0.00020                           | 4.3 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 5.68   | 0.545   | 0.00018                           | 3.9 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 6.38   | 0.617   | 0.00020                           | 4.4 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 7.18   | 0.699   | 0.00032                           | 7.0 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 8.23   | 0.810   | 0.00034                           | 7.5 x 10 <sup>-6</sup> | "                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 8.62   | 0.851   | 0.00035                           | 7.8 x 10 <sup>-6</sup> | A+B                                    |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| 8.66 <sup>b</sup>  | 0.856   | -                                 | -                      | B                                      |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| <sup>a</sup> A = Hf(IO <sub>3</sub> ) <sub>4</sub> B = NaIO <sub>3</sub> ·H <sub>2</sub> O   |   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| <sup>b</sup> For binary systems the compiler computes the following:   |   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| soly of NaIO <sub>3</sub> = 0.479 mol kg <sup>-1</sup>   |   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| soly of Hf(IO <sub>3</sub> ) <sub>4</sub> = 4.2 x 10 <sup>-6</sup> mol kg <sup>-1</sup>  |   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| <b>AUXILIARY INFORMATION</b>   |   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b>   | <b>SOURCE AND PURITY OF MATERIALS:</b>  |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| The isothermal method was used. Equilibrium was reached in 25-30 days. Samples of the coexisting phases were analyzed for sodium by emission spectrometry. The hafnium content was determined potentiometrically using Arsenazo III after reducing the iodate ion with hydroxylamine.  | C.p. grade NaIO <sub>3</sub> ·H <sub>2</sub> O was recrystallized from distilled water. Hafnium iodate was prepared by the action of aqueous iodic acid solution on freshly precipitated hafnium hydroxide (ref 1.)                   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| The composition in the solid phase was determined by the method of residues and the result was checked by X-ray analysis.  | <b>ESTIMATED ERROR:</b><br>Soly: within 1-3 % rel. % (emission spectrometry for Na).<br>Temp: precision ± 0.1 K.  |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |
| <b>REFERENCES:</b>   | 1. Deabrige, J.; Rohmer, R. <i>Bull. Soc. Chim. Fr.</i> 1968, 2, 521.   |                                   |                        |  |  |  |        |                     |        |                     |   |   |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |   |      |       |         |                        |     |                   |       |   |   |   |

| <b>COMPONENTS:</b><br>(1) Sodium iodate; $\text{NaIO}_3$ ; [7681-55-2]<br>(2) Iodic acid; $\text{HIO}_3$ ; [7782-68-5]<br>(3) Water; $\text{H}_2\text{O}$ ; [7732-18-5]  | <b>ORIGINAL MEASUREMENTS:</b><br>Meerburg, P.A.<br>Z. Anorg. Allg. Chem. <u>1905</u> , 45, 324-44. |                   |                  |                           |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
|--|--|-------------------|------------------|---------------------------|--|---------------------------|--------|------------------|--------|------------------|---|---|-------------------|-------|---|------|-------|------|-------|---|------|-------|-------|-------|---|------|-------|-------|-------|---|------|-------|-------|-------|------|------|-------|-------|-------|---|------|-------|-------|-------|-----|------|-------|-------|-------|---|------|-------|-------|-------|---|------|-------|-------|-------|---|------|-------|------|-------|---|------|-------|------|-------|---|-------|-------|------|-------|---|-------|-------|------|-------|-----|-------|-------|------|-------|---|-------|-------|------|-------|---|-------|-------|------|-------|---|-------|-------|------|-------|---|-------|-------|------|-------|---|-------|-------|------|-------|---|-------|-------|------|-------|---|-------|-------|------|-------|---|-------|-------|------|-------|-----|--------------------|-------|---|---|---|
| <b>VARIABLES:</b><br>T/K = 303<br>Composition  | <b>PREPARED BY:</b><br>Hiroshi Miyamoto  |                   |                  |                           |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| <b>EXPERIMENTAL VALUES:</b> Composition of saturated solutions at 30°C   |  |                   |                  |                           |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| <table border="1"> <thead> <tr> <th colspan="2">Iodic Acid</th> <th colspan="2">Sodium Iodate</th> <th rowspan="2">Nature of the solid phase</th> </tr> <tr> <th>mass %</th> <th>mol % (compiler)</th> <th>mass %</th> <th>mol % (compiler)</th> </tr> </thead> <tbody> <tr><td>0</td><td>0</td><td>9.36<sup>b</sup></td><td>0.931</td><td>A</td></tr> <tr><td>1.98</td><td>0.526</td><td>9.52</td><td>0.968</td><td>"</td></tr> <tr><td>4.86</td><td>0.576</td><td>10.22</td><td>1.077</td><td>"</td></tr> <tr><td>5.86</td><td>0.708</td><td>11.04</td><td>1.187</td><td>"</td></tr> <tr><td>7.40</td><td>0.915</td><td>11.60</td><td>1.275</td><td>A(m)</td></tr> <tr><td>9.73</td><td>1.280</td><td>14.73</td><td>1.722</td><td>"</td></tr> <tr><td>6.76</td><td>0.826</td><td>11.18</td><td>1.215</td><td>A+C</td></tr> <tr><td>6.75</td><td>0.824</td><td>11.10</td><td>1.205</td><td>"</td></tr> <tr><td>6.66</td><td>0.814</td><td>11.28</td><td>1.226</td><td>"</td></tr> <tr><td>7.80</td><td>0.955</td><td>10.30</td><td>1.121</td><td>C</td></tr> <tr><td>9.15</td><td>1.120</td><td>9.00</td><td>0.980</td><td>"</td></tr> <tr><td>9.93</td><td>1.222</td><td>8.71</td><td>0.953</td><td>"</td></tr> <tr><td>11.20</td><td>1.280</td><td>7.54</td><td>0.826</td><td>"</td></tr> <tr><td>11.89</td><td>1.471</td><td>7.21</td><td>0.793</td><td>C+D</td></tr> <tr><td>11.75</td><td>1.451</td><td>7.18</td><td>0.788</td><td>"</td></tr> <tr><td>14.62</td><td>1.822</td><td>5.65</td><td>0.629</td><td>D</td></tr> <tr><td>23.23</td><td>3.139</td><td>3.69</td><td>0.443</td><td>"</td></tr> <tr><td>32.68</td><td>4.920</td><td>2.91</td><td>0.389</td><td>"</td></tr> <tr><td>40.91</td><td>6.882</td><td>2.64</td><td>0.395</td><td>"</td></tr> <tr><td>46.62</td><td>8.567</td><td>2.67</td><td>0.436</td><td>"</td></tr> <tr><td>55.48</td><td>11.77</td><td>2.12</td><td>0.400</td><td>"</td></tr> <tr><td>65.47</td><td>16.94</td><td>1.83</td><td>0.420</td><td>"</td></tr> <tr><td>76.19</td><td>25.73</td><td>1.42</td><td>0.426</td><td>D+B</td></tr> <tr><td>76.70<sup>b</sup></td><td>25.21</td><td>0</td><td>0</td><td>B</td></tr> </tbody> </table> |  | Iodic Acid        |                  | Sodium Iodate             |  | Nature of the solid phase | mass % | mol % (compiler) | mass % | mol % (compiler) | 0 | 0 | 9.36 <sup>b</sup> | 0.931 | A | 1.98 | 0.526 | 9.52 | 0.968 | " | 4.86 | 0.576 | 10.22 | 1.077 | " | 5.86 | 0.708 | 11.04 | 1.187 | " | 7.40 | 0.915 | 11.60 | 1.275 | A(m) | 9.73 | 1.280 | 14.73 | 1.722 | " | 6.76 | 0.826 | 11.18 | 1.215 | A+C | 6.75 | 0.824 | 11.10 | 1.205 | " | 6.66 | 0.814 | 11.28 | 1.226 | " | 7.80 | 0.955 | 10.30 | 1.121 | C | 9.15 | 1.120 | 9.00 | 0.980 | " | 9.93 | 1.222 | 8.71 | 0.953 | " | 11.20 | 1.280 | 7.54 | 0.826 | " | 11.89 | 1.471 | 7.21 | 0.793 | C+D | 11.75 | 1.451 | 7.18 | 0.788 | " | 14.62 | 1.822 | 5.65 | 0.629 | D | 23.23 | 3.139 | 3.69 | 0.443 | " | 32.68 | 4.920 | 2.91 | 0.389 | " | 40.91 | 6.882 | 2.64 | 0.395 | " | 46.62 | 8.567 | 2.67 | 0.436 | " | 55.48 | 11.77 | 2.12 | 0.400 | " | 65.47 | 16.94 | 1.83 | 0.420 | " | 76.19 | 25.73 | 1.42 | 0.426 | D+B | 76.70 <sup>b</sup> | 25.21 | 0 | 0 | B |
| Iodic Acid   |  | Sodium Iodate     |                  | Nature of the solid phase |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| mass %   | mol % (compiler)   | mass %            | mol % (compiler) |                           |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 0  | 0  | 9.36 <sup>b</sup> | 0.931            | A                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 1.98   | 0.526  | 9.52              | 0.968            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 4.86   | 0.576  | 10.22             | 1.077            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 5.86   | 0.708  | 11.04             | 1.187            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 7.40   | 0.915  | 11.60             | 1.275            | A(m)                      |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 9.73   | 1.280  | 14.73             | 1.722            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 6.76   | 0.826  | 11.18             | 1.215            | A+C                       |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 6.75   | 0.824  | 11.10             | 1.205            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 6.66   | 0.814  | 11.28             | 1.226            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 7.80   | 0.955  | 10.30             | 1.121            | C                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 9.15   | 1.120  | 9.00              | 0.980            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 9.93   | 1.222  | 8.71              | 0.953            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 11.20  | 1.280  | 7.54              | 0.826            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 11.89  | 1.471  | 7.21              | 0.793            | C+D                       |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 11.75  | 1.451  | 7.18              | 0.788            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 14.62  | 1.822  | 5.65              | 0.629            | D                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 23.23  | 3.139  | 3.69              | 0.443            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 32.68  | 4.920  | 2.91              | 0.389            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 40.91  | 6.882  | 2.64              | 0.395            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 46.62  | 8.567  | 2.67              | 0.436            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 55.48  | 11.77  | 2.12              | 0.400            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 65.47  | 16.94  | 1.83              | 0.420            | "                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 76.19  | 25.73  | 1.42              | 0.426            | D+B                       |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| 76.70 <sup>b</sup>   | 25.21  | 0                 | 0                | B                         |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| <p><sup>a</sup> A = <math>\text{NaIO}_3 \cdot 1.5\text{H}_2\text{O}</math>; B = <math>\text{HIO}_3</math>; C = <math>\text{Na}_2\text{O} \cdot 2\text{I}_2\text{O}_5</math>; D = <math>\text{NaIO}_3 \cdot 2\text{HIO}_3</math>.</p> <p><sup>b</sup> For binary systems the compiler computes the following:<br/>           soly of <math>\text{HIO}_3</math> = 18.71 mol kg<sup>-1</sup><br/>           soly of <math>\text{NaIO}_3</math> = 0.522 mol kg<sup>-1</sup></p>  |  |                   |                  |                           |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br><p>A mixture of <math>\text{NaIO}_3</math>, <math>\text{HIO}_3</math> and water was placed in a bottle and the bottle agitated in a thermostat for a week or more at a desired temperature. Equilibrium was established from supersaturation.</p> <p>The iodic acid and sodium iodate contents were detd as follows: an excess of KI was added to an aliquot of satd sln, and the <math>\text{HIO}_3</math> content detd by titration of the iodine liberated with standard sodium thiosulfate. Dil sulfuric acid was then added to the solution and the iodine liberated was again titrated with sodium thiosulfate to obtain the total iodate concentration.</p> <p>The sodium iodate concentration was calculated from the difference between the second and the first titration.</p> <p>Composition of solid phases determined by the method of residues.</p>  | <b>SOURCE AND PURITY OF MATERIALS</b><br>Nothing specified.  |                   |                  |                           |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| <b>ESTIMATED ERROR:</b><br>Nothing specified.  |  |                   |                  |                           |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |
| <b>COMMENTS AND/OR ADDITIONAL DATA:</b><br>(mass % units)  |  |                   |                  |                           |  |                           |        |                  |        |                  |   |   |                   |       |   |      |       |      |       |   |      |       |       |       |   |      |       |       |       |   |      |       |       |       |      |      |       |       |       |   |      |       |       |       |     |      |       |       |       |   |      |       |       |       |   |      |       |       |       |   |      |       |      |       |   |      |       |      |       |   |       |       |      |       |   |       |       |      |       |     |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |   |       |       |      |       |     |                    |       |   |   |   |

| <b>COMPONENTS:</b><br>(1) Sodium iodate; $\text{NaIO}_3$ ; [7681-55-2]<br>(2) Iodic acid; $\text{HIO}_3$ ; [7782-68-5]<br>(3) Water; $\text{H}_2\text{O}$ ; [7732-18-5]   |                     | <b>ORIGINAL MEASUREMENTS:</b><br>Shibuya, M.; Watanobe, T.<br><i>Denki Kagaku</i> <u>1967</u> , 35, 550-8  |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
|---|---------------------|--|---------------------|-------------------------------|---|-------------------------------|---|------|-------|-------------------|-------|-------|---|------|-------|------|-------|-------|---|------|-------|------|-------|-------|---|------|-------|------|-------|-------|---|------|-------|------|-------|-------|---|------|-------|------|-------|-------|---|------|-------|------|-------|-------|---|------|-------|------|-------|-------|-----|------|-------|------|-------|-------|---|------|------|------|-------|-------|-----|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|-------|---|-------|-------|------|-------|---|---|-------|-------|------|-------|---|---|--|--|
| <b>VARIABLES:</b><br>Composition<br>T/K = 288.2   |                     | <b>PREPARED BY:</b><br>Hiroshi Miyamoto and Mark Salomon   |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| <b>EXPERIMENTAL VALUES:</b>   |                     | Composition of saturated solutions at 15.0°C   |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| <table border="1"> <thead> <tr> <th>Iodic acid<br/>mass %</th> <th>mol %<br/>(compiler)</th> <th>Sodium Iodate<br/>mass %</th> <th>mol %<br/>(compiler)</th> <th>density<br/><math>\text{g cm}^{-3}</math></th> <th>Nature of the<br/>solid phase<sup>a</sup></th> </tr> </thead> <tbody> <tr><td>0.00</td><td>0.000</td><td>5.87<sup>b</sup></td><td>0.564</td><td>1.051</td><td>A</td></tr> <tr><td>0.62</td><td>0.067</td><td>5.87</td><td>0.568</td><td>1.057</td><td>"</td></tr> <tr><td>1.79</td><td>0.197</td><td>5.87</td><td>0.574</td><td>1.070</td><td>"</td></tr> <tr><td>2.59</td><td>0.287</td><td>5.92</td><td>0.584</td><td>1.077</td><td>"</td></tr> <tr><td>3.81</td><td>0.428</td><td>5.90</td><td>0.589</td><td>1.089</td><td>"</td></tr> <tr><td>5.12</td><td>0.583</td><td>5.99</td><td>0.606</td><td>1.103</td><td>"</td></tr> <tr><td>5.66</td><td>0.649</td><td>6.14</td><td>0.626</td><td>1.109</td><td>"</td></tr> <tr><td>7.63</td><td>0.895</td><td>6.38</td><td>0.665</td><td>1.132</td><td>A+B</td></tr> <tr><td>8.06</td><td>0.947</td><td>6.18</td><td>0.646</td><td>1.135</td><td>B</td></tr> <tr><td>9.11</td><td>1.08</td><td>5.64</td><td>0.592</td><td>1.143</td><td>B+C</td></tr> <tr><td>10.57</td><td>1.256</td><td>4.74</td><td>0.501</td><td>1.145</td><td>C</td></tr> <tr><td>12.21</td><td>1.459</td><td>3.68</td><td>0.391</td><td>1.152</td><td>"</td></tr> <tr><td>19.16</td><td>2.435</td><td>2.43</td><td>0.274</td><td>1.215</td><td>"</td></tr> <tr><td>33.45</td><td>5.018</td><td>1.88</td><td>0.251</td><td>-</td><td>"</td></tr> <tr><td>43.26</td><td>7.444</td><td>1.82</td><td>0.278</td><td>-</td><td>"</td></tr> </tbody> </table> |                     | Iodic acid<br>mass %   | mol %<br>(compiler) | Sodium Iodate<br>mass %       | mol %<br>(compiler)                       | density<br>$\text{g cm}^{-3}$ | Nature of the<br>solid phase <sup>a</sup> | 0.00 | 0.000 | 5.87 <sup>b</sup> | 0.564 | 1.051 | A | 0.62 | 0.067 | 5.87 | 0.568 | 1.057 | " | 1.79 | 0.197 | 5.87 | 0.574 | 1.070 | " | 2.59 | 0.287 | 5.92 | 0.584 | 1.077 | " | 3.81 | 0.428 | 5.90 | 0.589 | 1.089 | " | 5.12 | 0.583 | 5.99 | 0.606 | 1.103 | " | 5.66 | 0.649 | 6.14 | 0.626 | 1.109 | " | 7.63 | 0.895 | 6.38 | 0.665 | 1.132 | A+B | 8.06 | 0.947 | 6.18 | 0.646 | 1.135 | B | 9.11 | 1.08 | 5.64 | 0.592 | 1.143 | B+C | 10.57 | 1.256 | 4.74 | 0.501 | 1.145 | C | 12.21 | 1.459 | 3.68 | 0.391 | 1.152 | " | 19.16 | 2.435 | 2.43 | 0.274 | 1.215 | " | 33.45 | 5.018 | 1.88 | 0.251 | - | " | 43.26 | 7.444 | 1.82 | 0.278 | - | " |  |  |
| Iodic acid<br>mass %  | mol %<br>(compiler) | Sodium Iodate<br>mass %  | mol %<br>(compiler) | density<br>$\text{g cm}^{-3}$ | Nature of the<br>solid phase <sup>a</sup> |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 0.00  | 0.000               | 5.87 <sup>b</sup>  | 0.564               | 1.051                         | A   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 0.62  | 0.067               | 5.87   | 0.568               | 1.057                         | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 1.79  | 0.197               | 5.87   | 0.574               | 1.070                         | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 2.59  | 0.287               | 5.92   | 0.584               | 1.077                         | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 3.81  | 0.428               | 5.90   | 0.589               | 1.089                         | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 5.12  | 0.583               | 5.99   | 0.606               | 1.103                         | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 5.66  | 0.649               | 6.14   | 0.626               | 1.109                         | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 7.63  | 0.895               | 6.38   | 0.665               | 1.132                         | A+B                                       |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 8.06  | 0.947               | 6.18   | 0.646               | 1.135                         | B   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 9.11  | 1.08                | 5.64   | 0.592               | 1.143                         | B+C                                       |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 10.57   | 1.256               | 4.74   | 0.501               | 1.145                         | C   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 12.21   | 1.459               | 3.68   | 0.391               | 1.152                         | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 19.16   | 2.435               | 2.43   | 0.274               | 1.215                         | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 33.45   | 5.018               | 1.88   | 0.251               | -                             | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| 43.26   | 7.444               | 1.82   | 0.278               | -                             | "   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| <sup>a</sup> A = $\text{NaIO}_3 \cdot 5\text{H}_2\text{O}$ ;    B = $2\text{NaIO}_3 \cdot \text{I}_2\text{O}_5$ ;    C = $\text{NaIO}_3 \cdot \text{I}_2\text{O}_5$   |                     |  |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| <sup>b</sup> For the binary system the compiler computes the following:<br>$\text{Soly of NaIO}_3 = 0.315 \text{ mol kg}^{-1}$  |                     |  |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| <b>AUXILLARY INFORMATION</b>  |                     |  |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>Isothermal method by three techniques depending upon mole fraction, $x$ , of $\text{HIO}_3$ . (1) For $x = 0$ to 0.574. Excess acid added to $\text{NaIO}_3$ sln and stirred for 5 h. (2) For $x = 0.574$ to 0.646. Aq acid sln for $x = 0.638$ was cooled to obtain $\text{HIO}_3$ crystals. The crystals were added to an unsatd sln of $\text{NaIO}_3$ , and the mixture was stirred for a long time. (3) $x = 0.646$ to 1.0. Method essentially identical to (2) except that the acid crystals pptd from a sln where $x = 0.883$ , and stirring time was stated as 48 h. After equil was established and the slns allowed to settle, aliquots of satd sln were withdrawn with a pipet and weighed. The densities of the satd slns were detd. The total iodate concn was detd iodometrically, and the $\text{HIO}_3$ detd by acid-base titrn. Sodium was detd by difference. The composition of the solid phase was detd as follows: chem analyses were used to detn the acid and $\text{NaIO}_3$ contents, and thermogravimetry and NMR were used to detn the water content.  |                     | <b>SOURCE AND PURITY OF MATERIALS:</b><br>Sodium iodate was recryst three times from an aqueous sln prepd by electrolytic oxidation of iodine in alkaline sln. Iodic acid was prepd by ion exchange as follows: aq $\text{NaIO}_3$ sln was passed through a column of $\text{H}^+$ -resin (Amberlite IR 120), and the eluate was concentrated to about 30 % acid content by evaporation. The acid content was detd by acid-base titration. |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
|   |                     | <b>ESTIMATED ERROR:</b><br>Soly: rel error probably $\pm 0.2 \%$ (compilers).<br>Temp: precision $\pm 0.05 \text{ K}$ .  |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |
|   |                     | <b>REFERENCES:</b>   |                     |                               |   |                               |   |      |       |                   |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |   |      |       |      |       |       |     |      |       |      |       |       |   |      |      |      |       |       |     |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |       |   |       |       |      |       |   |   |       |       |      |       |   |   |  |  |

|  |   |
|--|---|
| <b>COMPONENTS:</b><br>(1) Sodium iodate; NaIO <sub>3</sub> ; [6781-55-2]<br>(2) 6,7,10,17,18,20,21-Octahydrodibenzo [b,k] [1,4,7,10,13,16] hexaoxacyclooctadecin (dibenzo-18-crown-6); C <sub>20</sub> H <sub>24</sub> O <sub>6</sub> ; [14187-32-7]<br>(3) Methanol; CH <sub>4</sub> O; [67-56-1]   | <b>ORIGINAL MEASUREMENTS:</b><br>Kolthoff, I.M.; Chantooni, Jr., M.K.<br><i>Anal. Chem.</i> <u>1980</u> , 52, 1039-44.  |
| <b>VARIABLES:</b><br>T/K = 298   | <b>PREPARED BY:</b><br>Hiroshi Miyamoto   |
| <b>EXPERIMENTAL VALUES:</b><br>The solubility product of NaIO <sub>3</sub> in methanol at 25°C is<br>$1.5 \times 10^{-7} \text{ mol}^2 \text{ dm}^{-6}$<br><b>COMMENTS AND/OR ADDITIONAL DATA:</b><br>In solutions saturated with respect to NaIO <sub>3</sub> and dibenzo-18-crown-6 (DB-18), the authors studied the equilibrium<br>$\text{Na}^+ + \text{L} = \text{LNa}^+ ; K_f(\text{LNa}^+) = [\text{L}][\text{Na}^+]/[\text{LNa}^+]$ where L = (ligand) concentration of dibenzo-18-crown-6. Details of experimental method presumed to be similar to those for KIO <sub>3</sub> -DB-18-MeOH system (compiled elsewhere in this volume). Authors only report $\log [K_f(\text{LNa}^+)/\text{mol}^{-1} \text{ dm}^3] = 4.4$ . |   |
| <b>AUXILIARY INFORMATION</b>   |   |
| <b>METHOD/APPARATUS/PROCEDURE:</b><br>A Markson No. 1001 Na <sup>+</sup> specific ion electrode used to determine a <sub>Na<sup>+</sup></sub> . The electrode was calibrated and found to respond in a Nernstian manner.   | <b>SOURCE AND PURITY OF MATERIALS:</b><br>Fisher "c.p." grade NaIO <sub>3</sub> was recrystallized 3 times from distilled water, and dried at 70°C.<br>(Fisher "Spectro purity" grade) was distilled from magnesium turnings. |
| <b>ESTIMATED ERROR:</b><br>Nothing specified.  |   |
| <b>REFERENCES:</b>   |   |